

The role of multiphase instabilities in Nature's extremes

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SIGMA

Simulations
of Geophysical
Multi-phAse flows



ICE



FIRE



ROCK



WATER

Fracture or flow?



FRACTURE

but:

Aseismic deformation and creep?



FLOW

but:

Eruption speeds of 100s m/s?

Fracture ~~or~~ and? flow?



FRACTURE

but:

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Eruption speeds of 100s m/s?

Fracture ~~or~~ and? flow?



FRACTURE

Sliding over a hydrologically flushed fault zone



FLOW

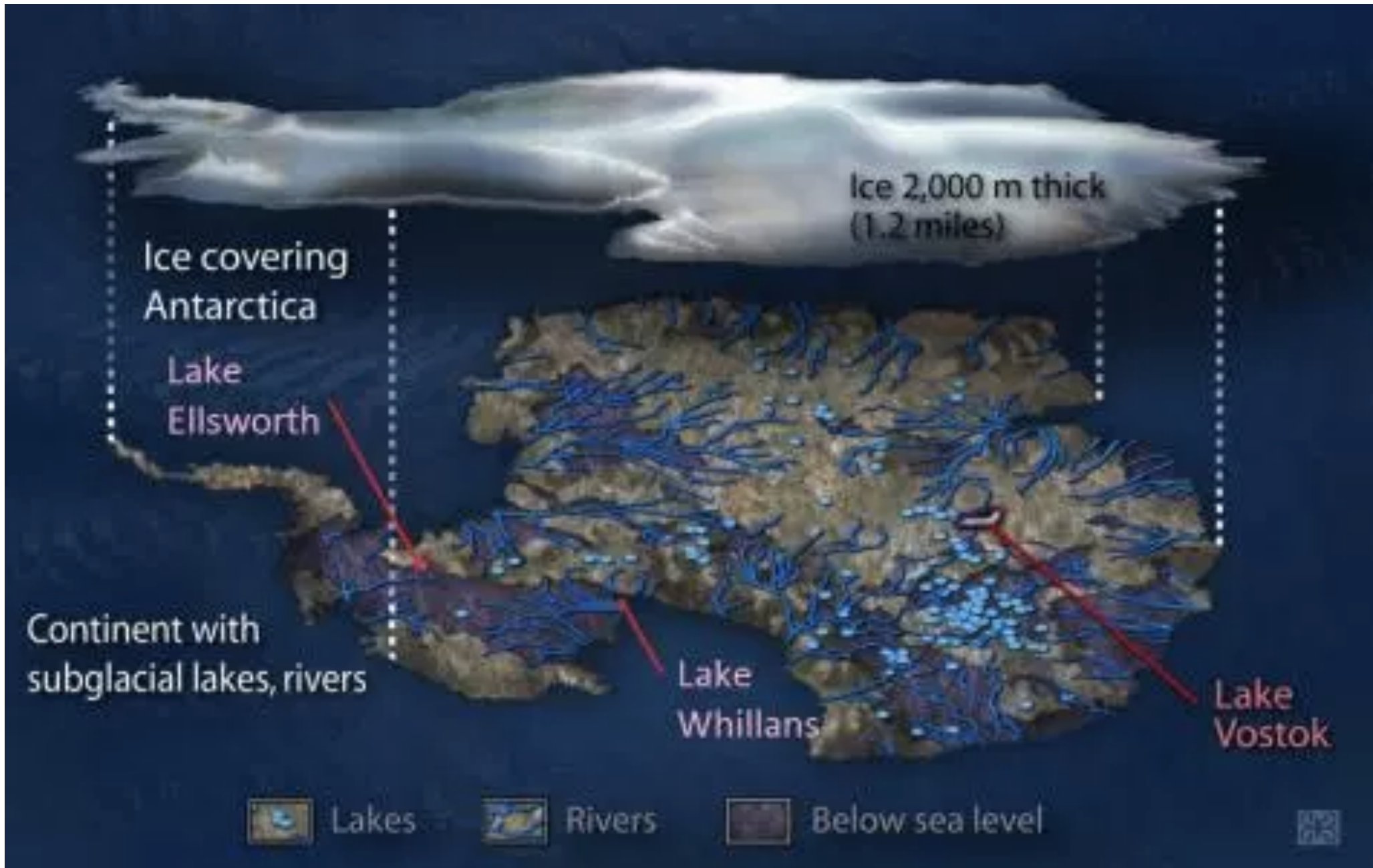
Stability of a solid matrix experiencing sustained flow

Fracture ~~or~~ and? flow?



FRACTURE

Sliding over a hydrologically
flushed fault zone



Artistic representation by Zina Deretsky, National Science Foundation

Figure by Cooper Elsworth

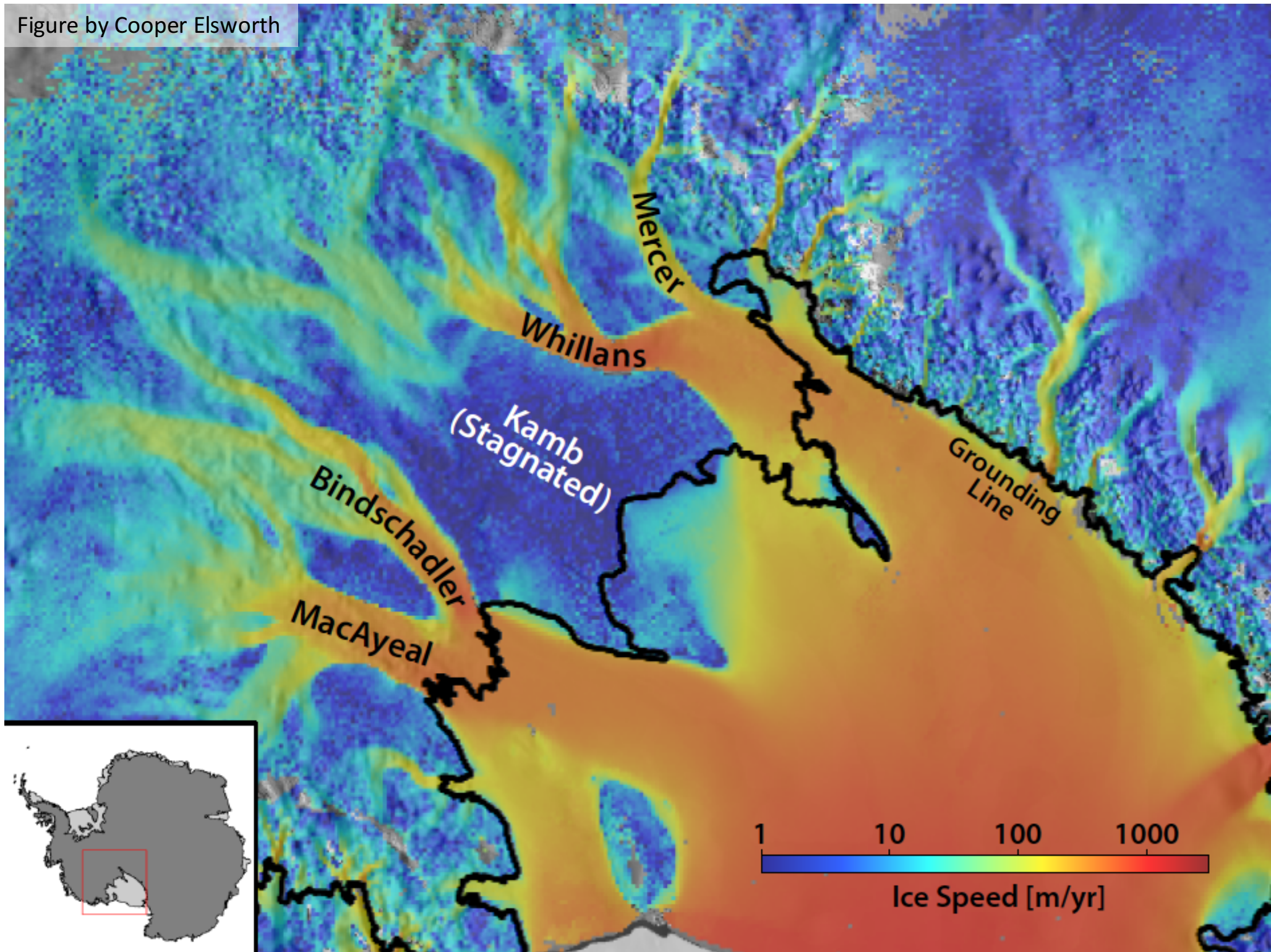
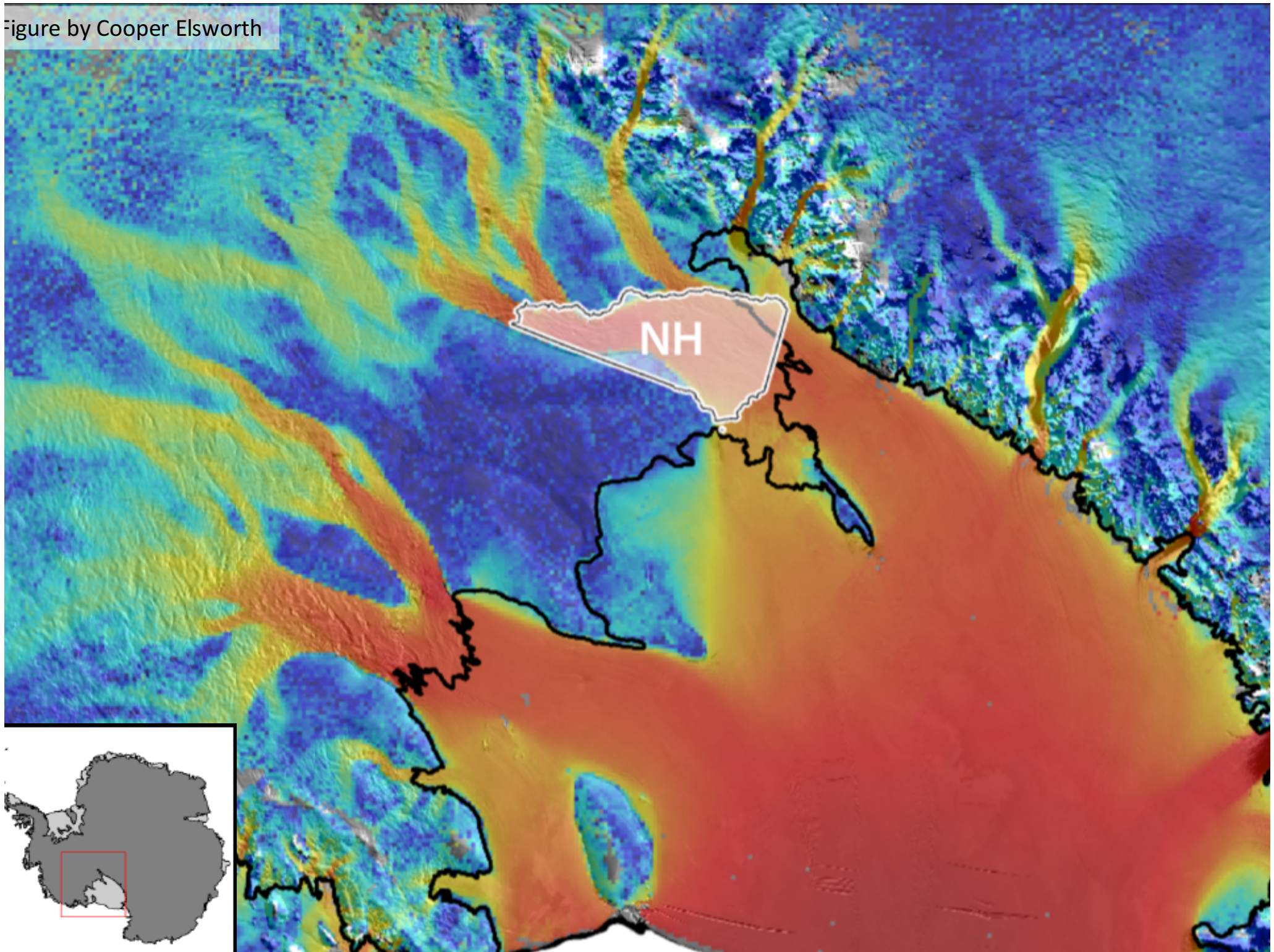


Figure by Cooper Elsworth





Sliding: localized deformation



Flow: distributed deformation

Figure by Cooper Elsworth

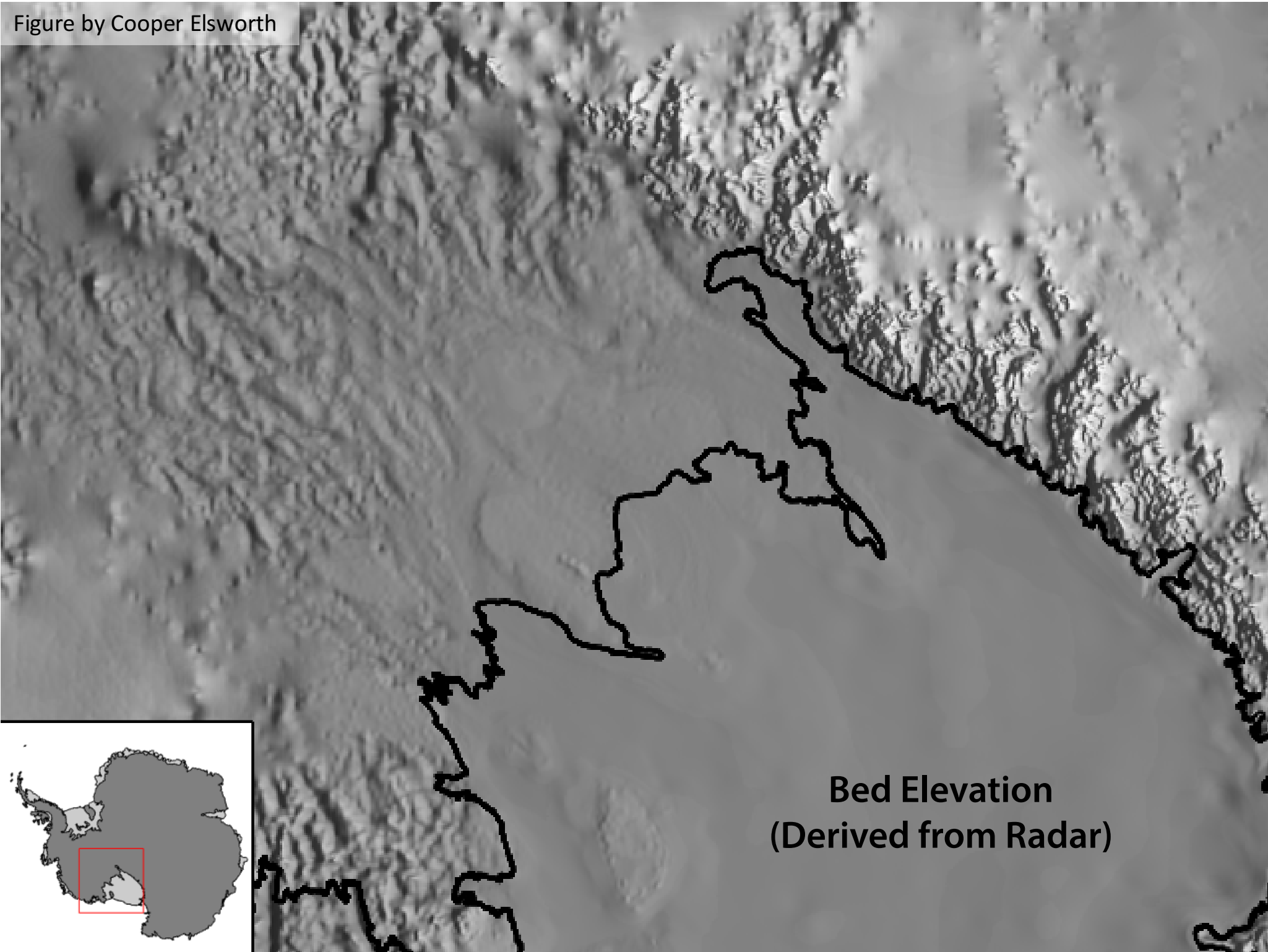


Figure by Cooper Elsworth

$$\tau_* = f(\sigma_n - p)$$

**Bed Elevation
(Derived from Radar)**



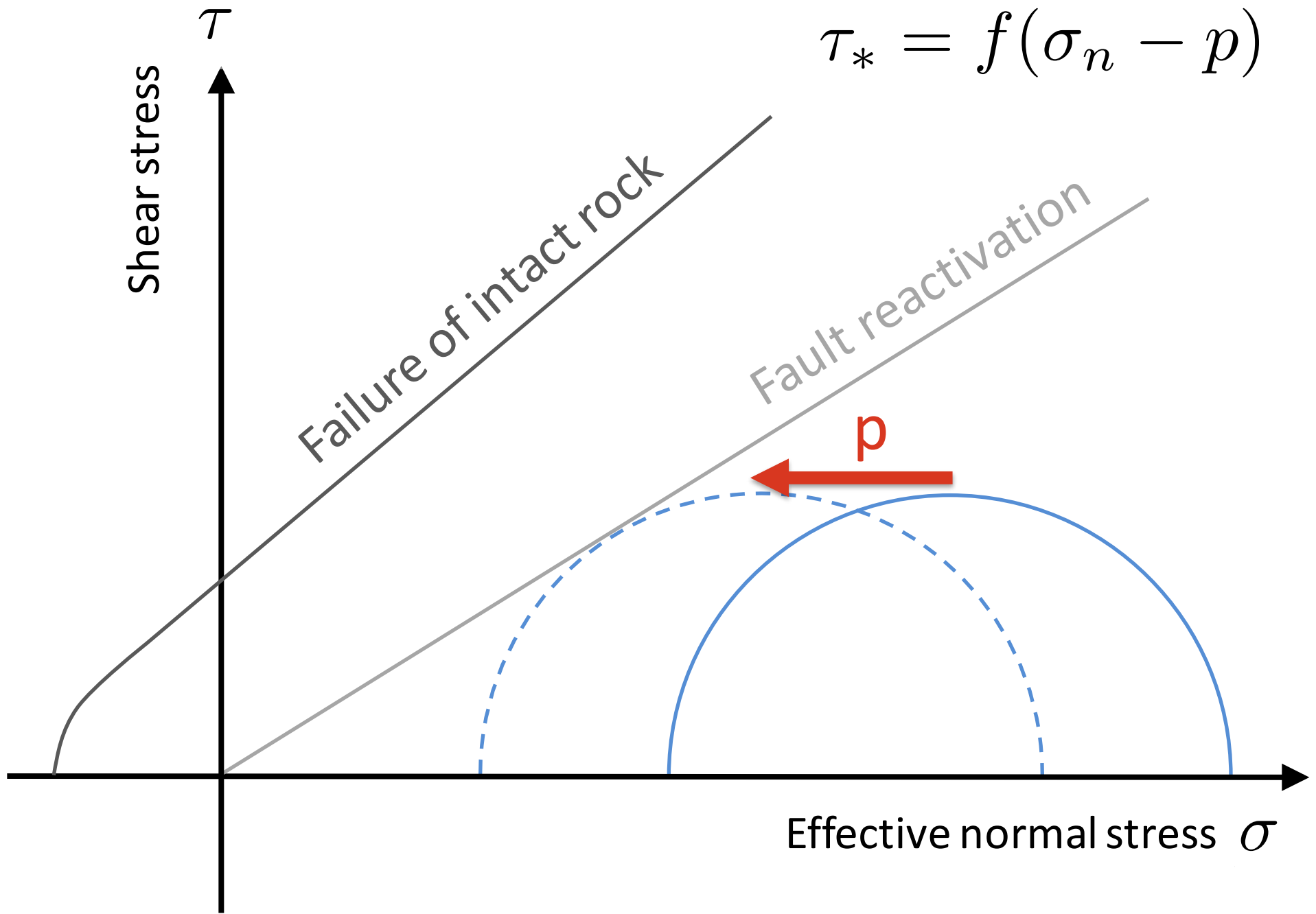
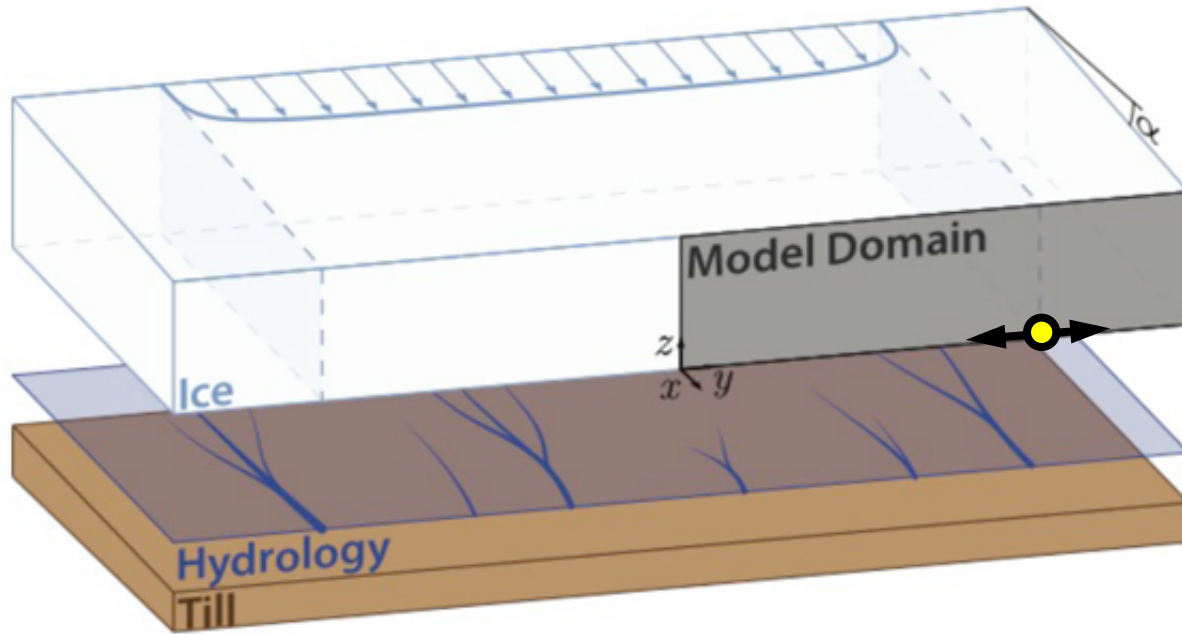




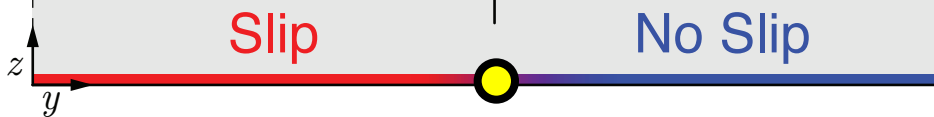
Photo courtesy of Mike Hambrey, Taylor Glacier, Antarctica, 1987



Cooper Elsworth

Mechanical Model

$$\frac{\partial}{\partial y} \left(\mu \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial z} \left(\mu \frac{\partial u}{\partial z} \right) = -\rho g \sin(\alpha)$$



Thermal Model

$$\frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + 2\tau_E \dot{\epsilon}_E = 0$$



Fully Coupled

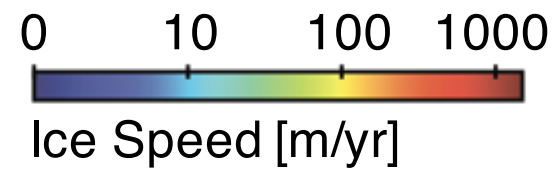
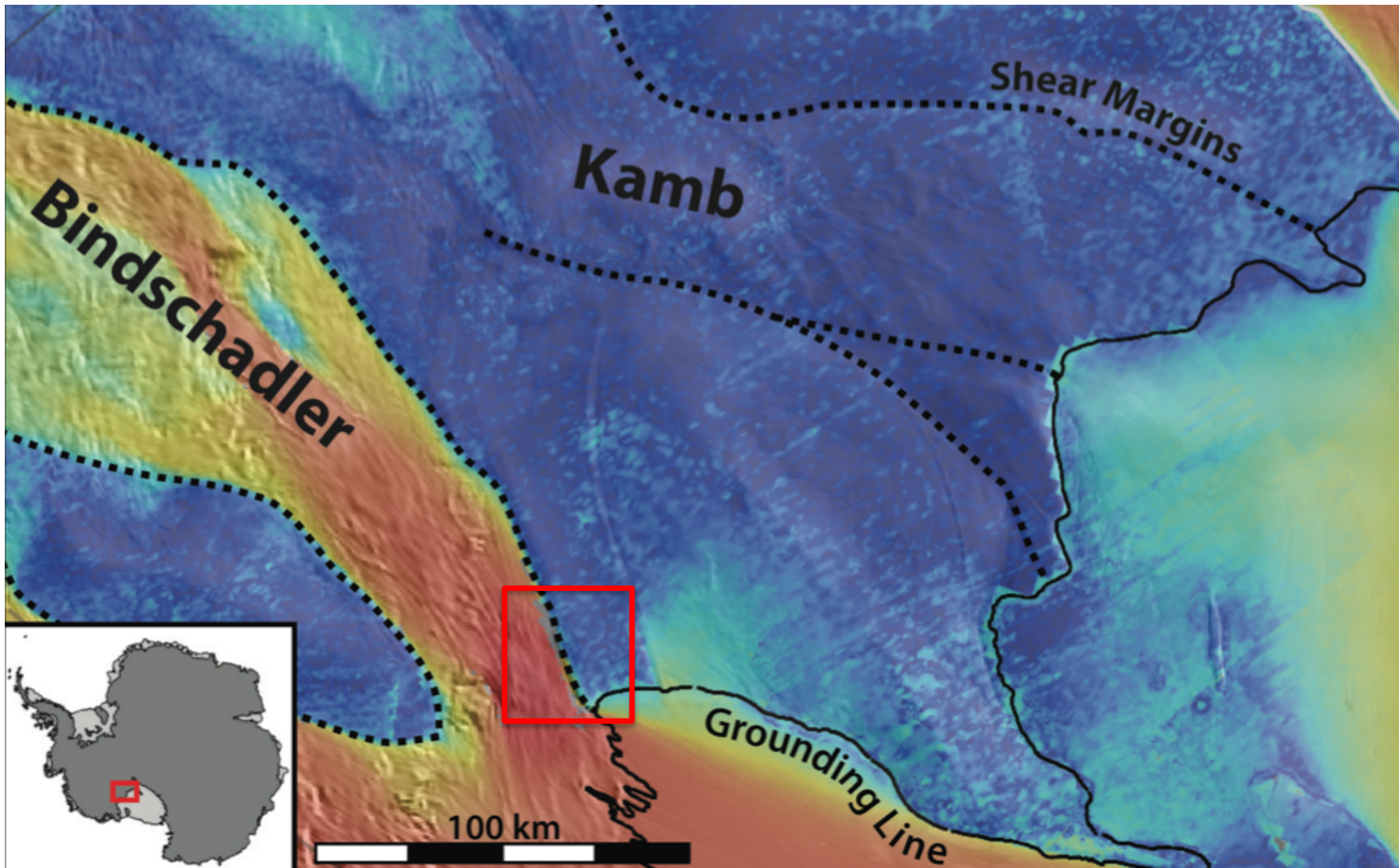
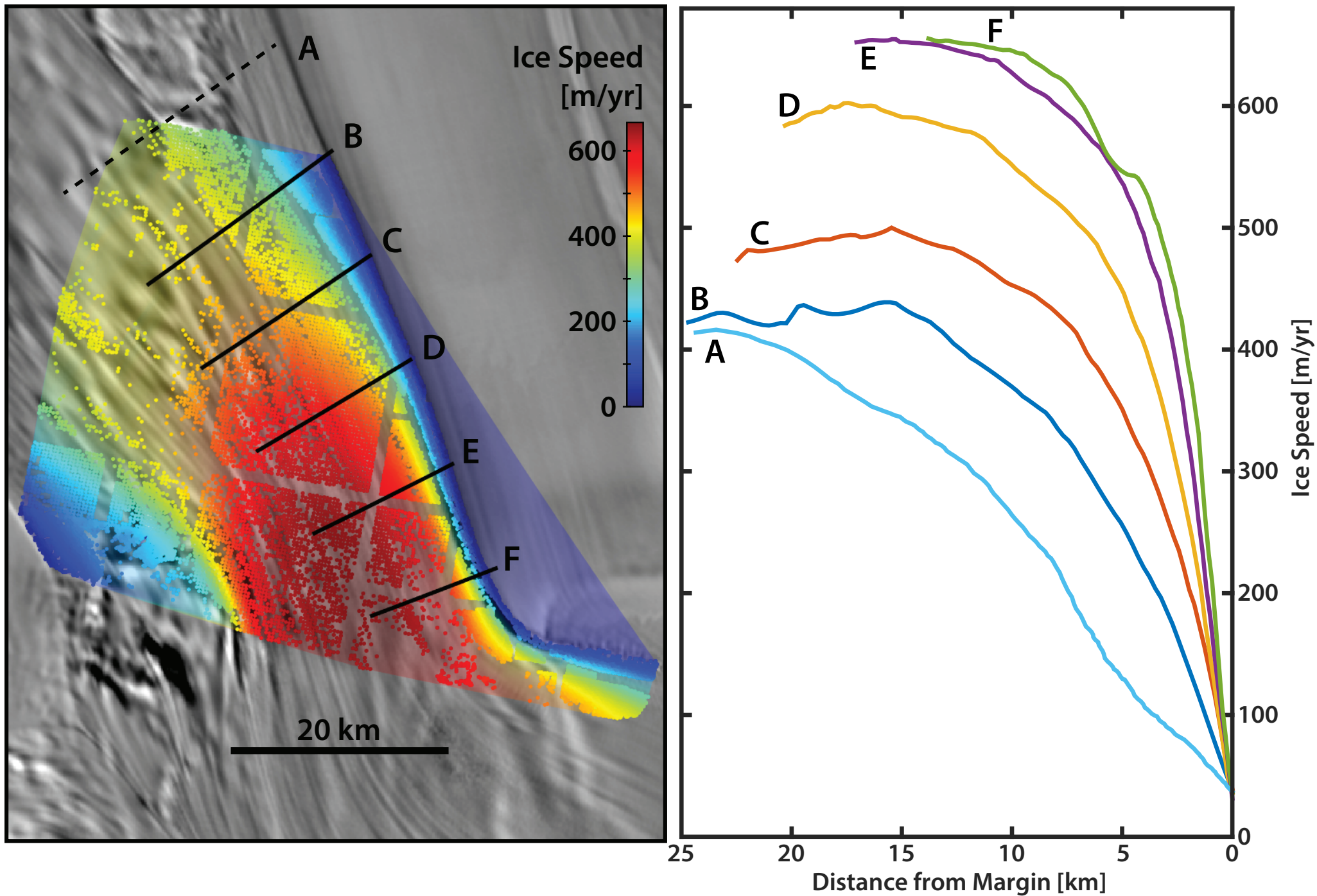
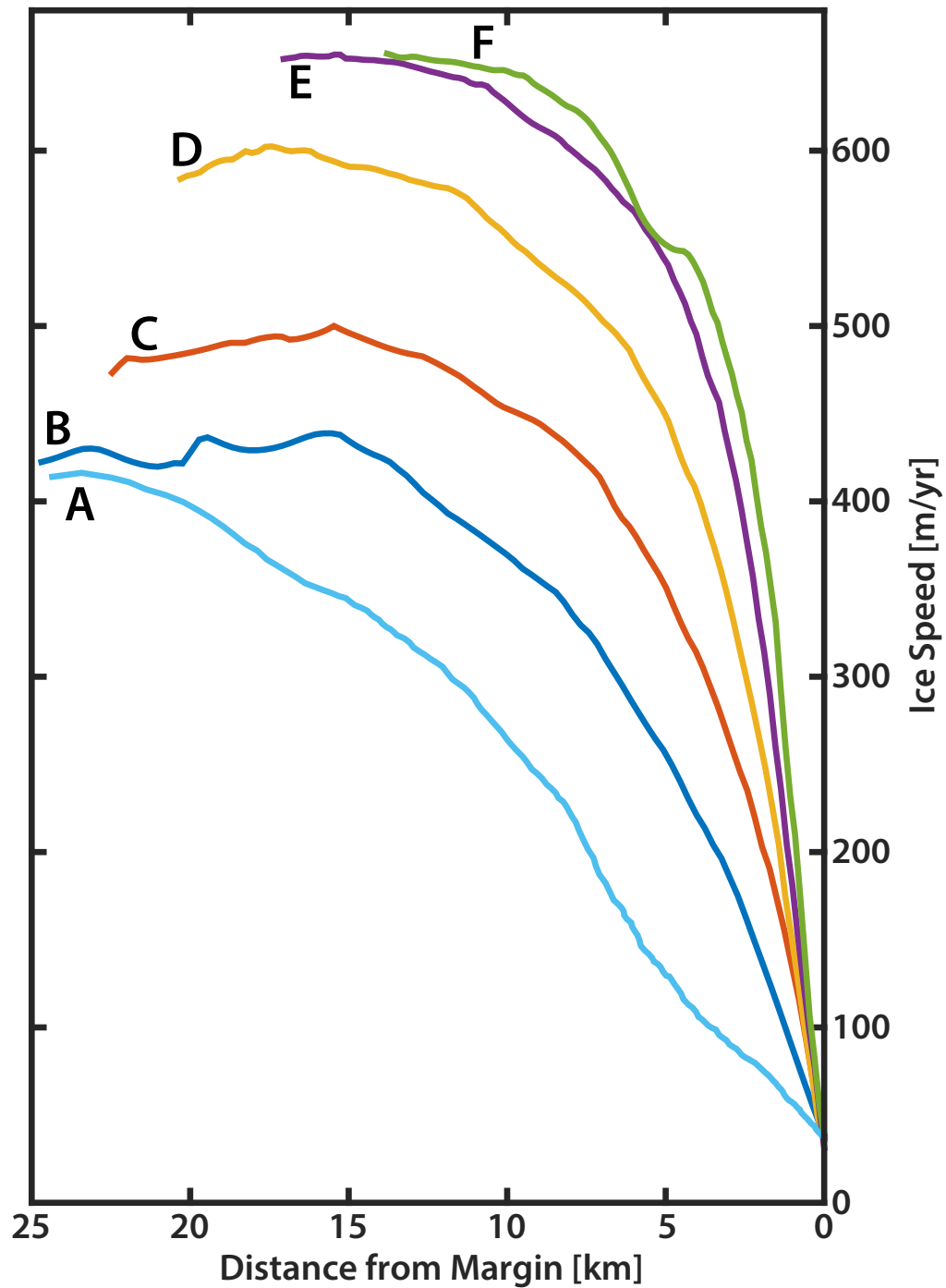
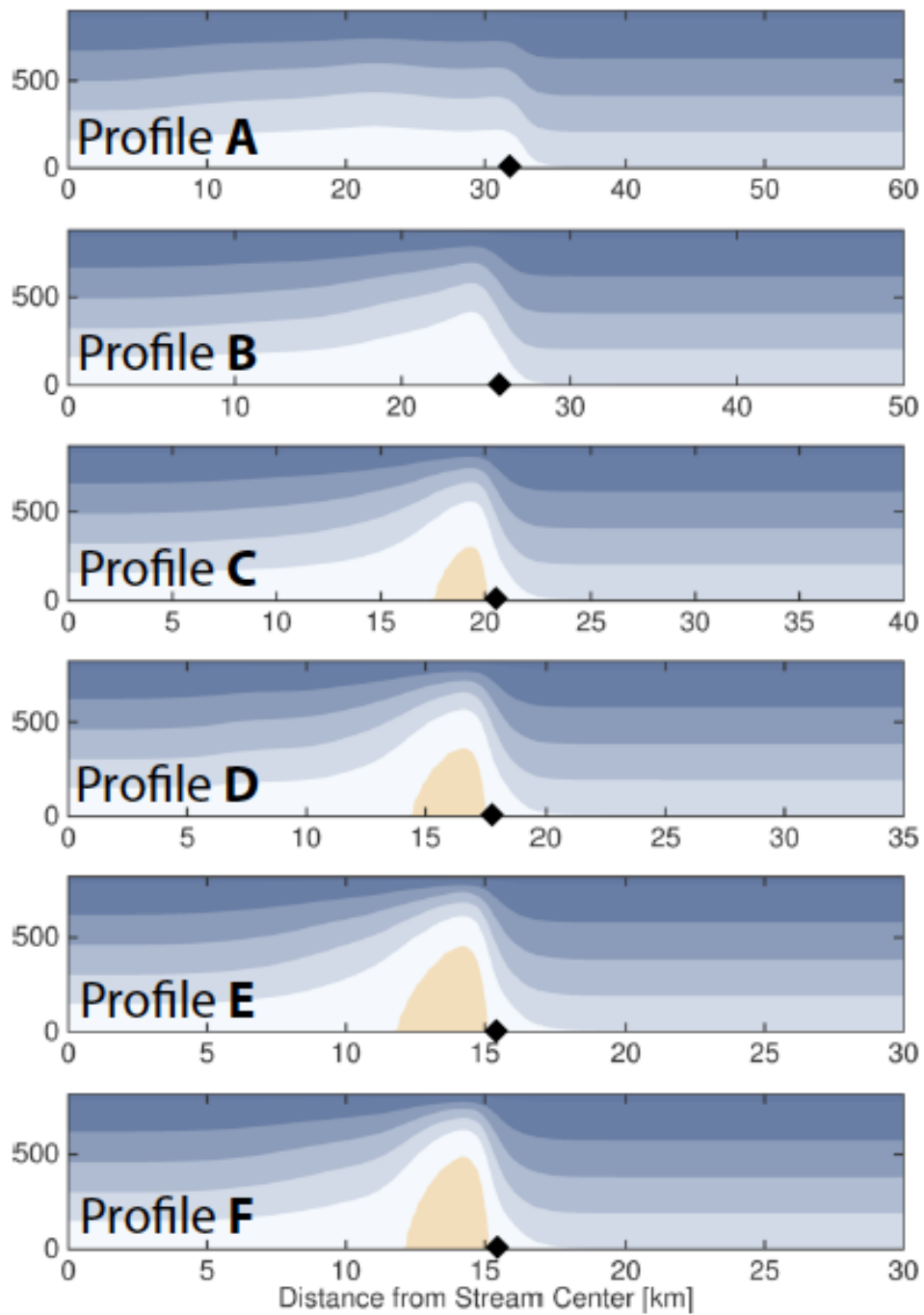


Figure by Cooper Elsworth

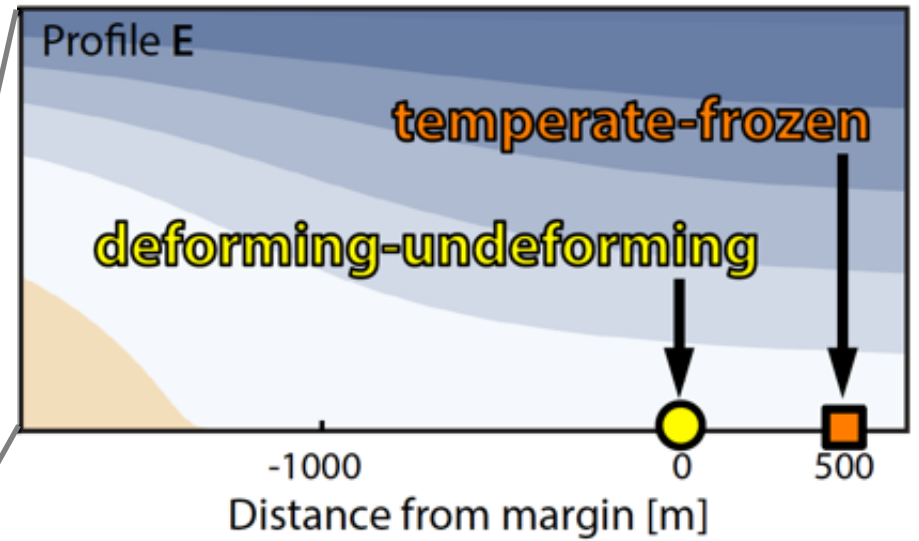
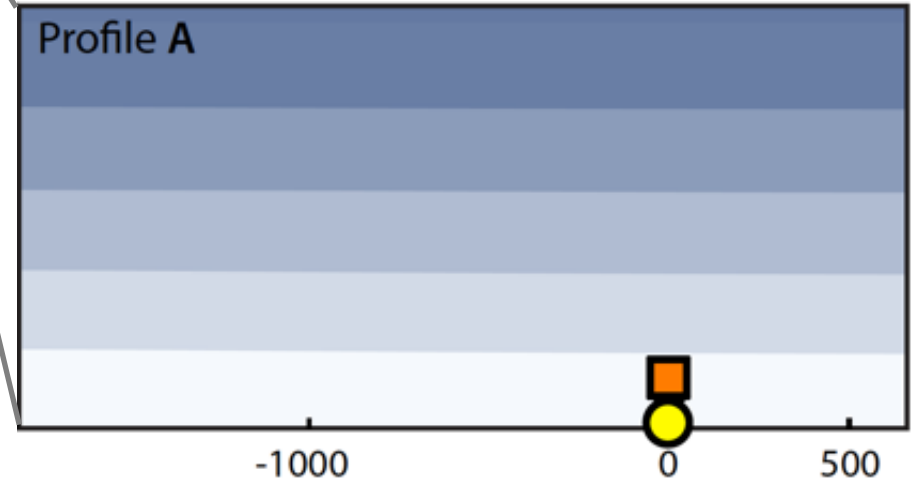
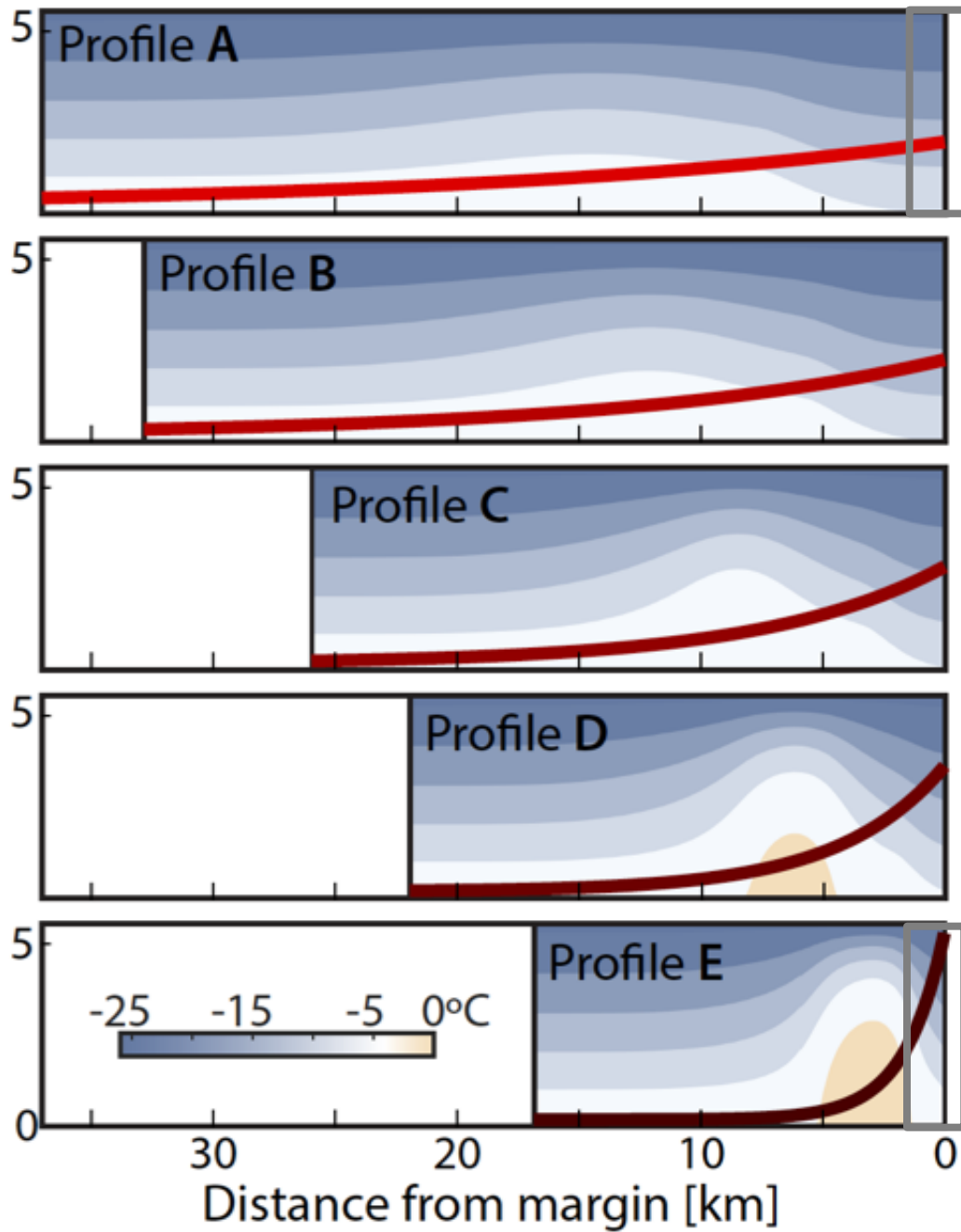


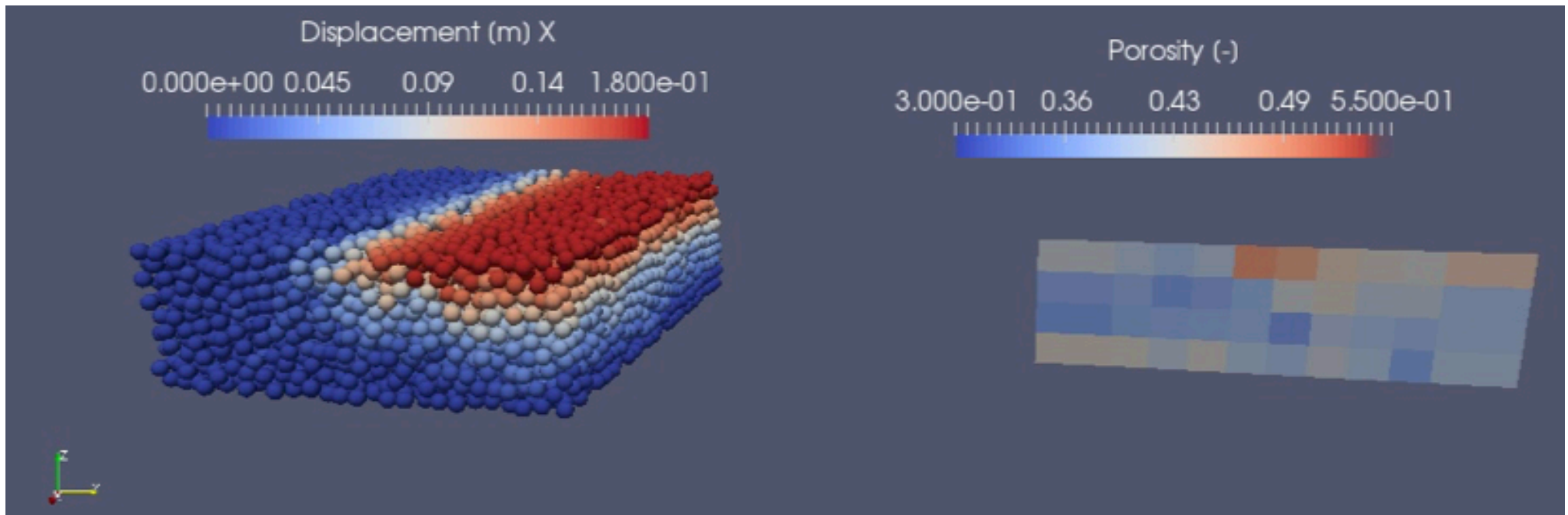
Data from NSIDC, Scambos et al., 1994



Simulations by Cooper Elsworth; see Elsworth and Suckale, 2016

Normalized Basal Strength
 $(\tau_c / \rho g H \alpha)$





Grains:

$$\frac{\partial^2 \mathbf{x}^i}{\partial t^2} m^i = \mathbf{f}_g^i + \sum_{j \in N} \left(\mathbf{f}_n^{i,j} + \mathbf{f}_t^{i,j} \right) + \mathbf{f}_f^i$$

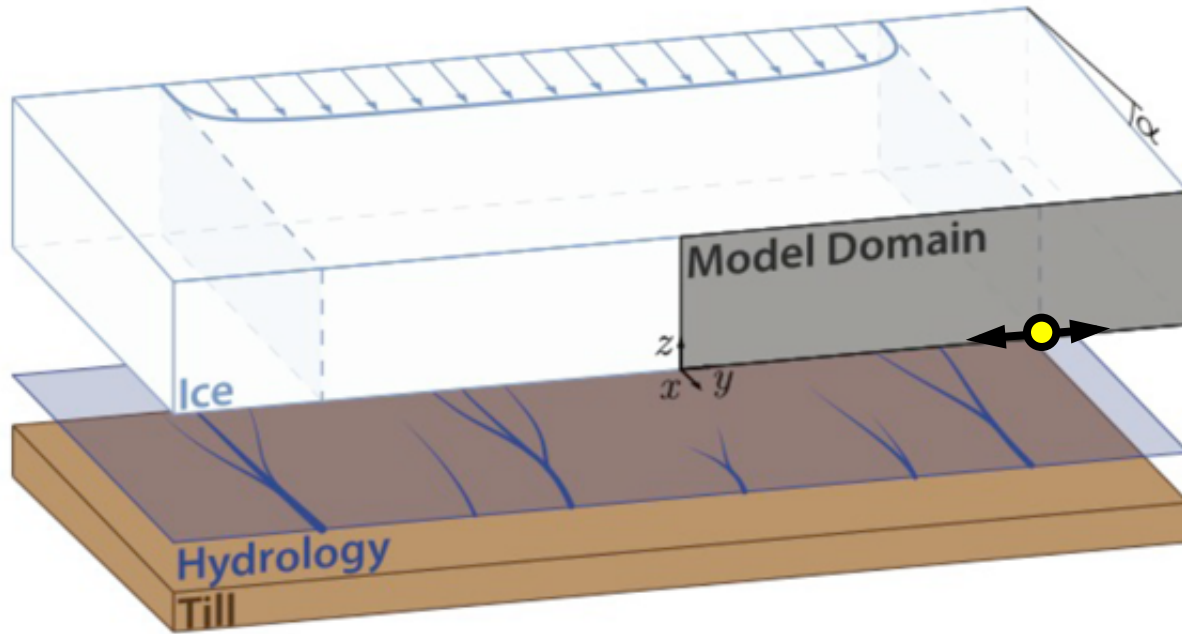
Water:

$$\frac{\partial P}{\partial t} = \frac{1}{\beta \Phi \eta} \nabla \cdot [k \nabla P] - \frac{1}{\beta \Phi (1 - \Phi)} \frac{\partial \Phi}{\partial t}$$

➔ Flow channelization occurs first at the shear margin

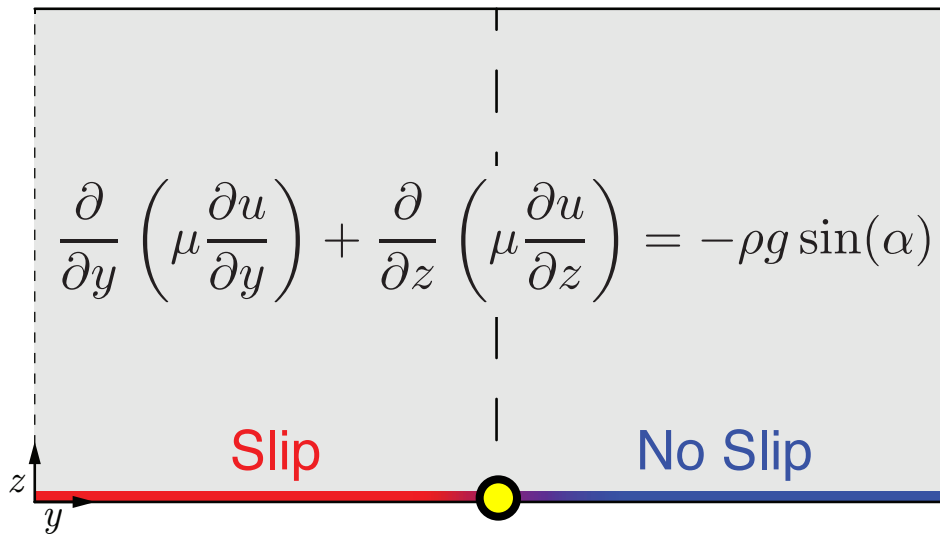


Indraneel Kasmalkar

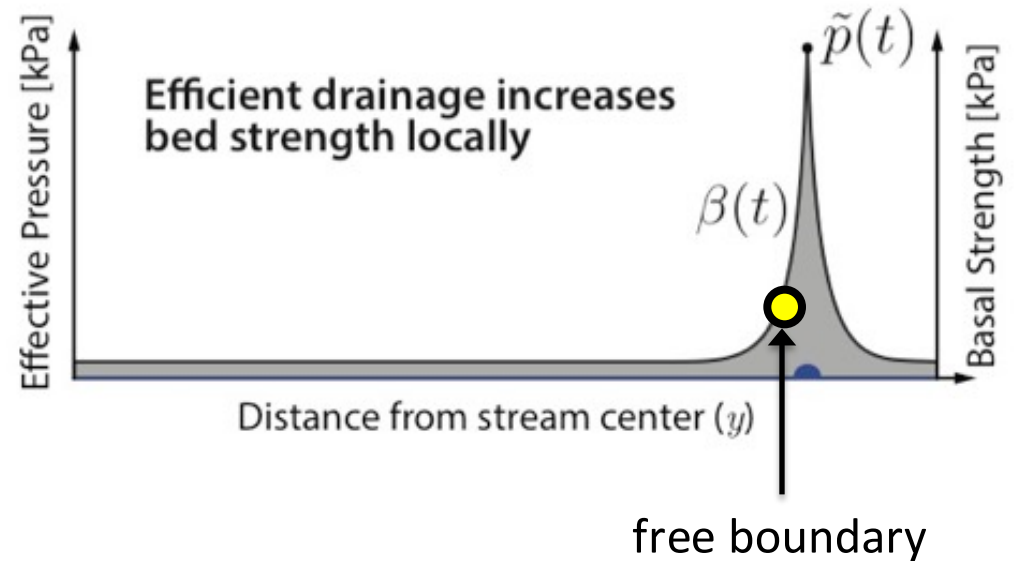


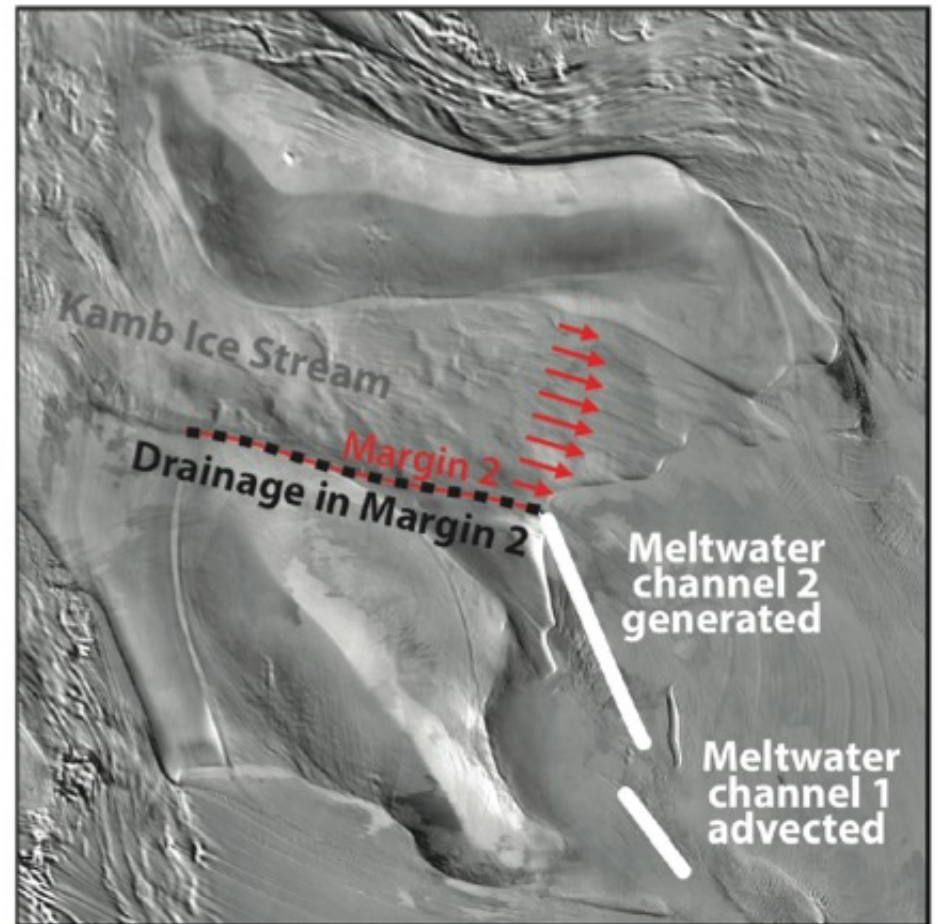
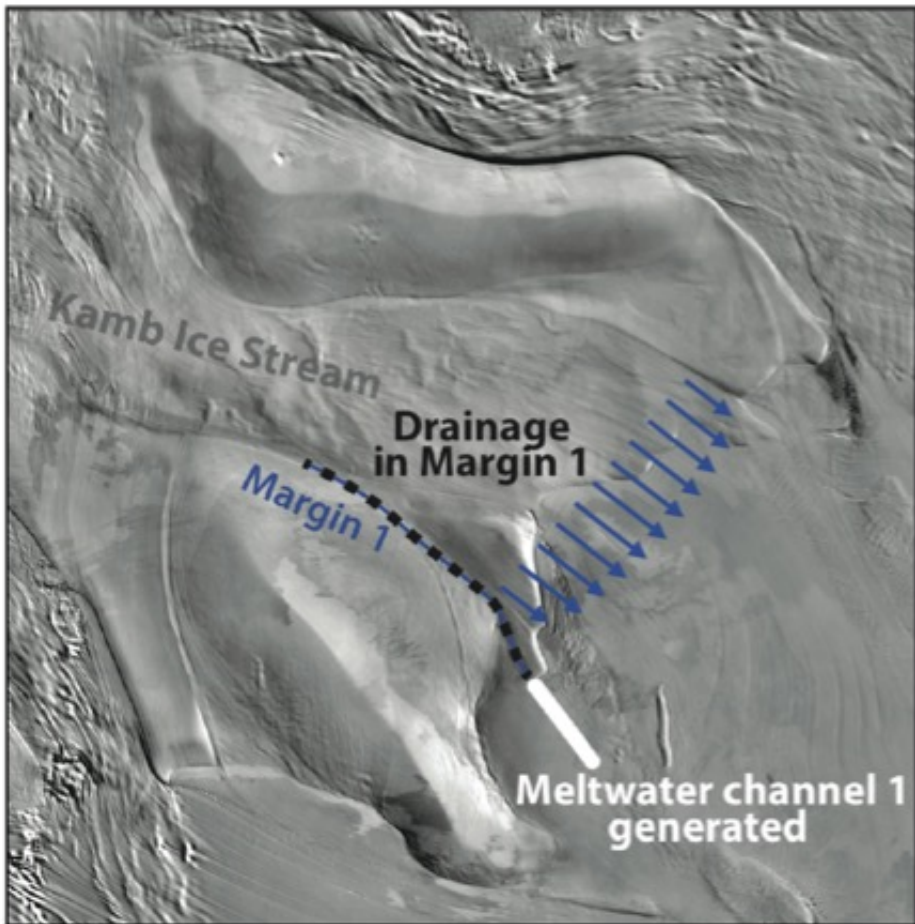
Cooper Elsworth

Mechanical Model



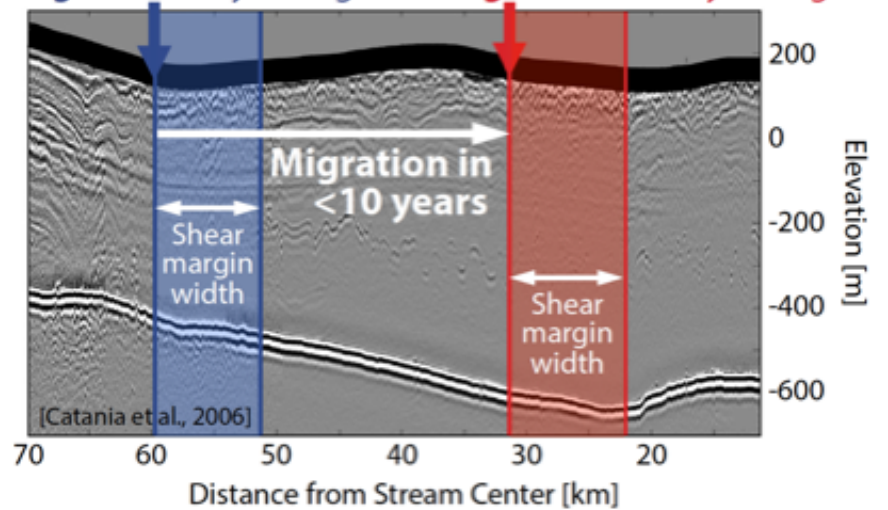
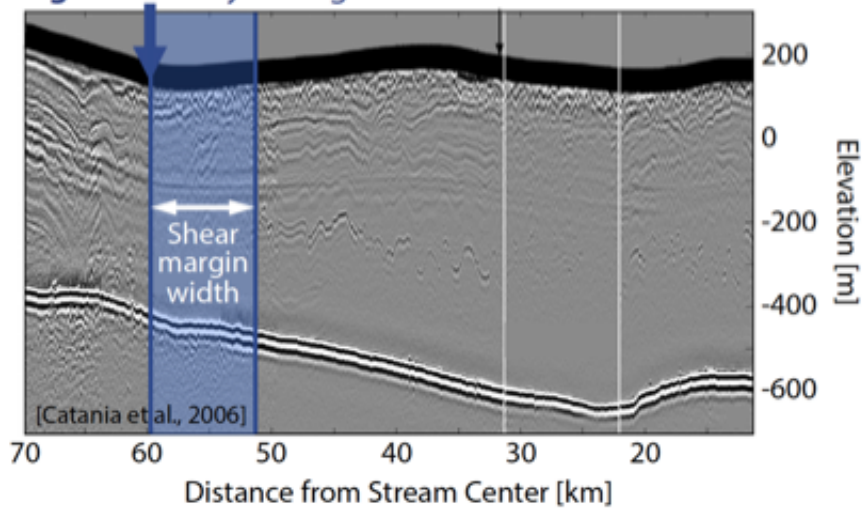
$$\tau_* = f(\sigma_n - p)$$



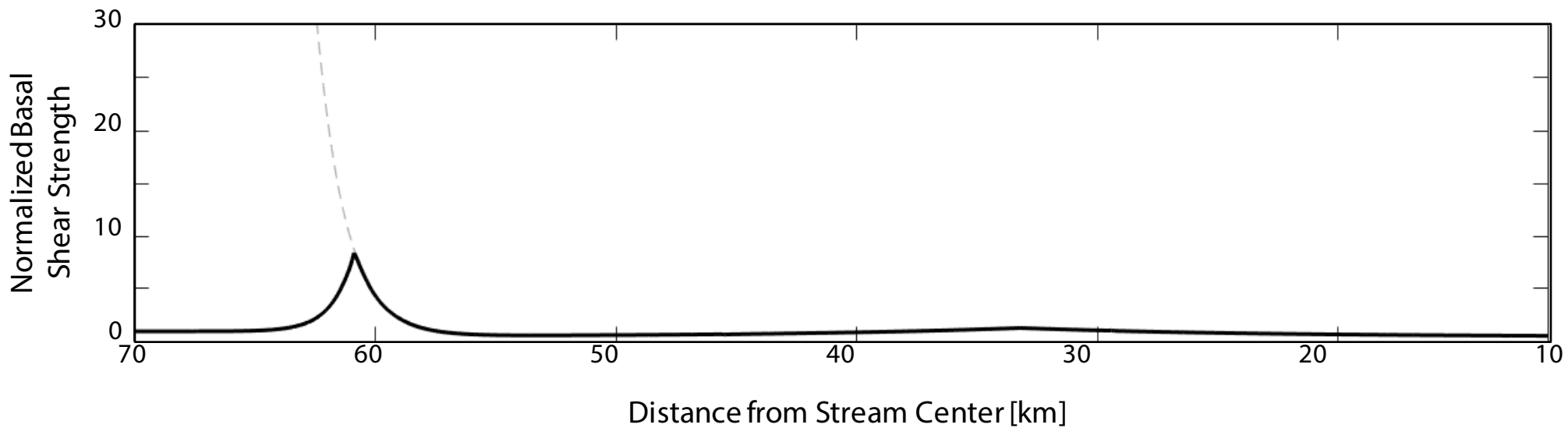
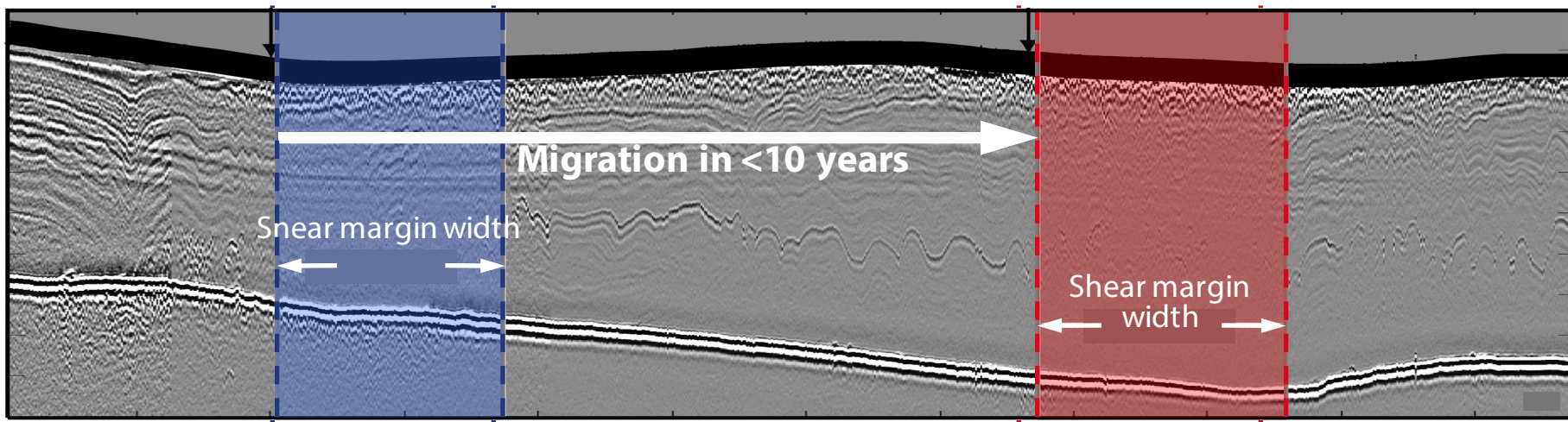


Margin 1: >340 years ago

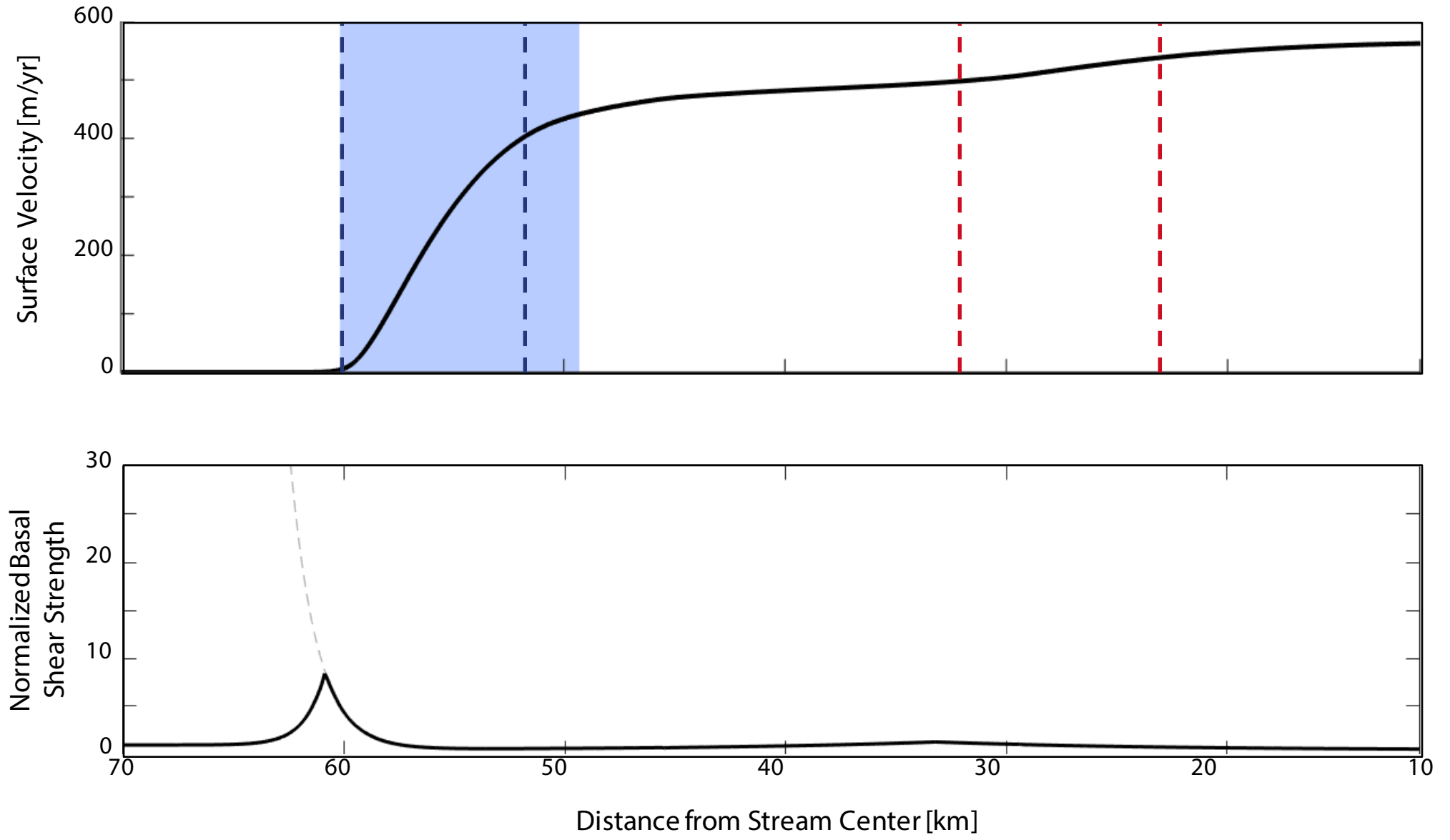
Margin 1: >340 years ago Margin 2: 330-150 years ago



Simulations by Cooper Elsworth; see Elsworth and Suckale, 2016

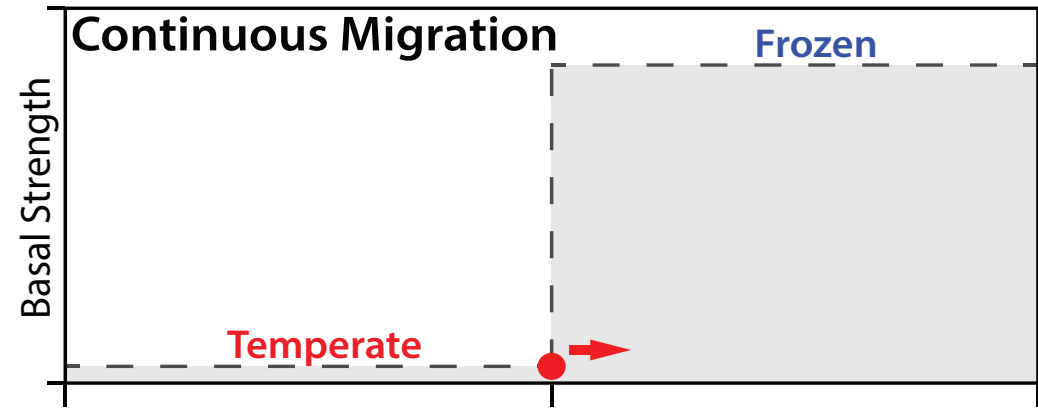
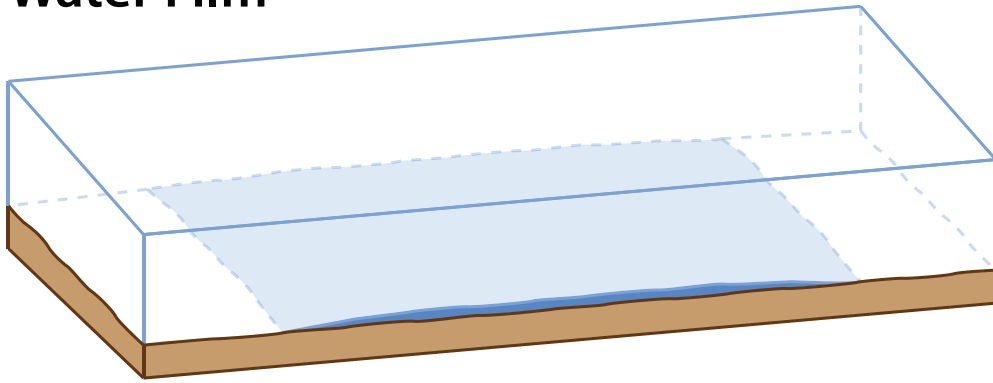


Simulations by Cooper Elsworth; see Elsworth and Suckale, 2016

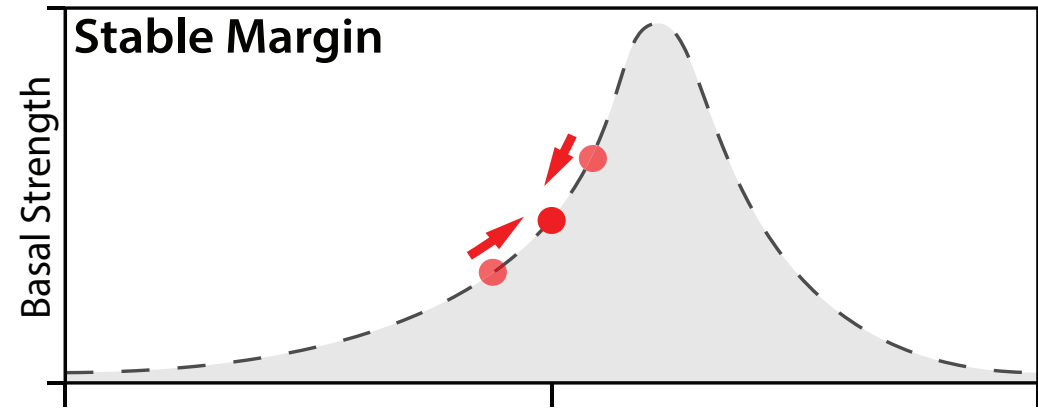
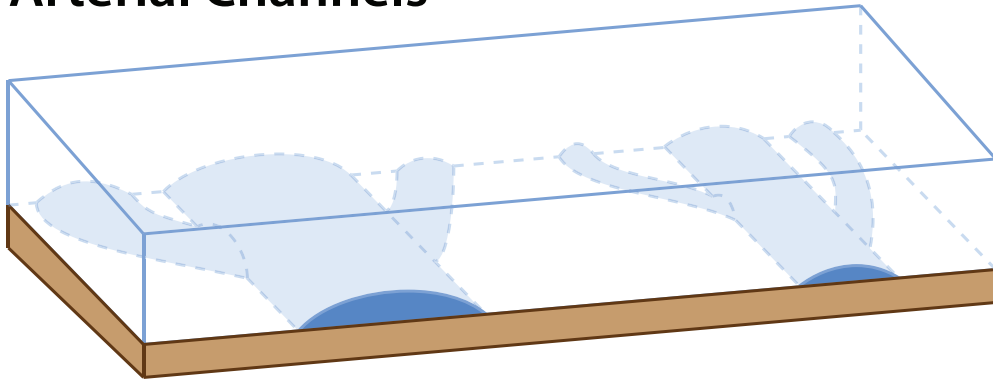


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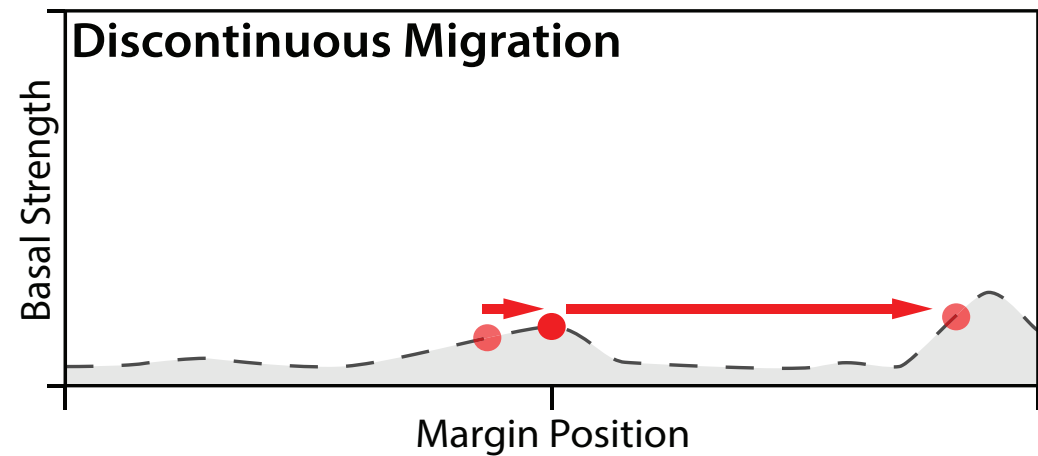
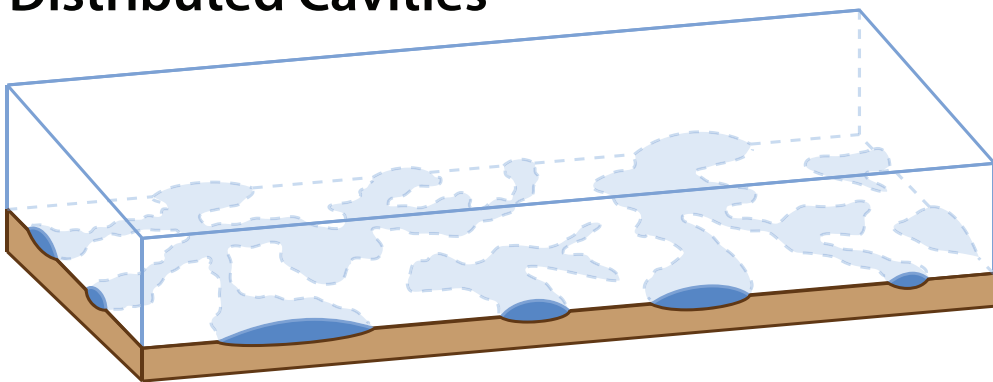
Water Film



Arterial Channels



Distributed Cavities



Fracture ~~or~~ flow? and?



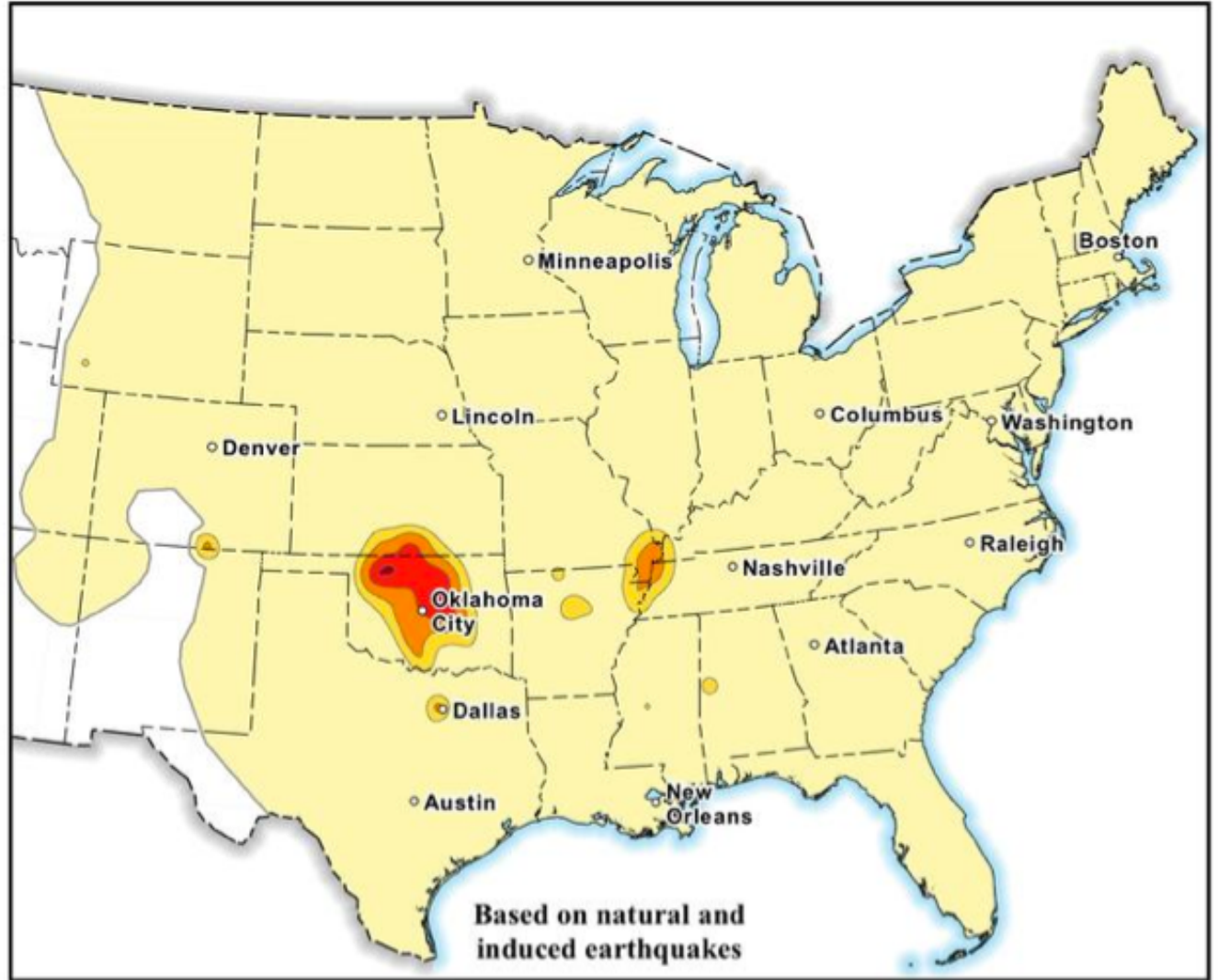
FRACTURE

Sliding over a hydrologically flushed fault zone

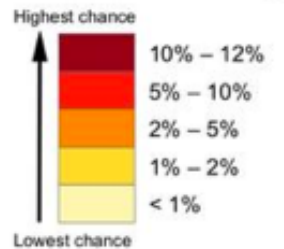
→ Flow creates a patchy fault surface (here: dry patches act as asperities, lakes are zones of free slip)

→ Flow introduces a different time scale that can lead to rapid rearrangement of the slipping zone.

USGS Forecast for Damage from Natural and Induced Earthquakes in 2016



Chance of damage



Injection rate in million of barrels ($\approx 10^8$ liter) per month

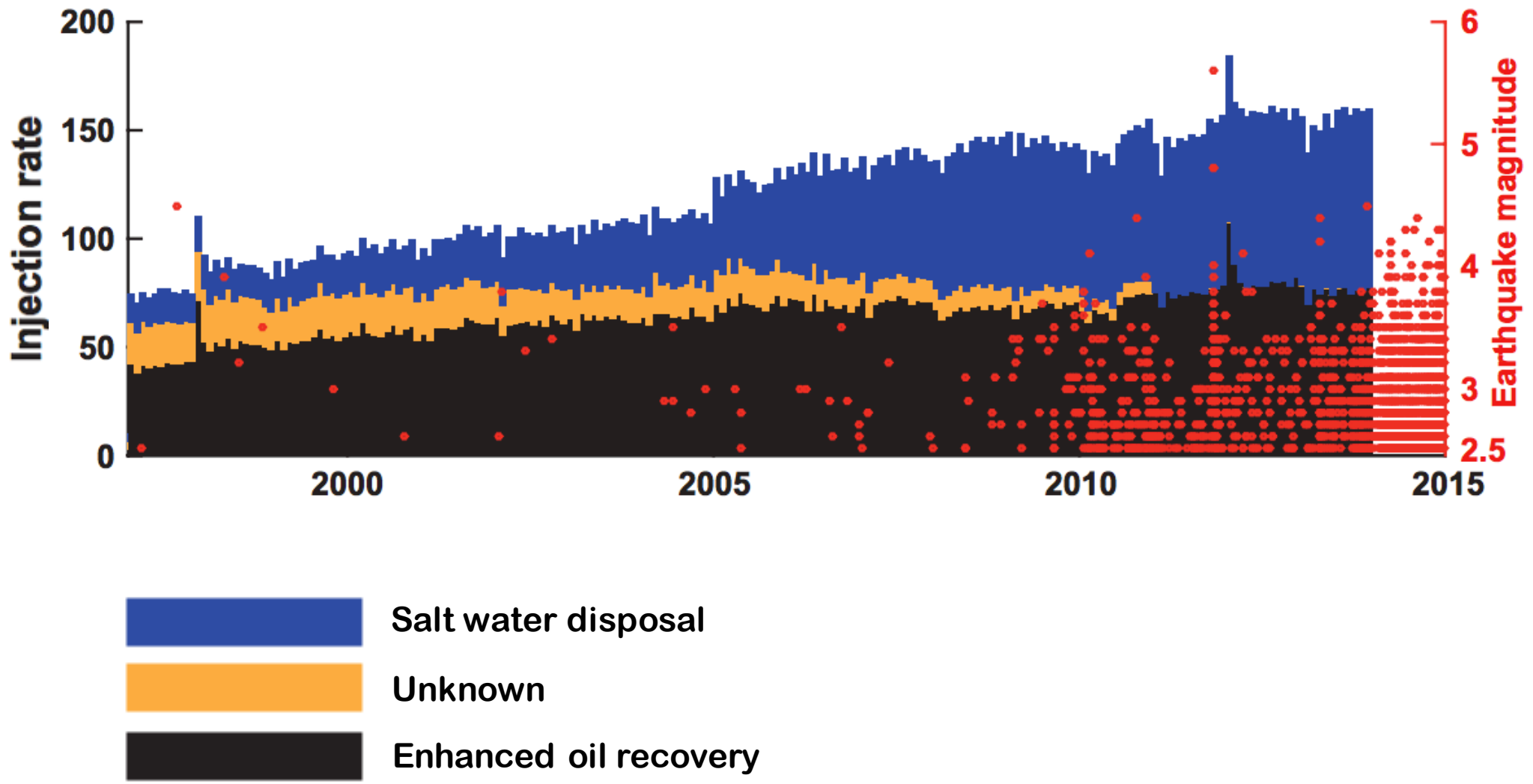
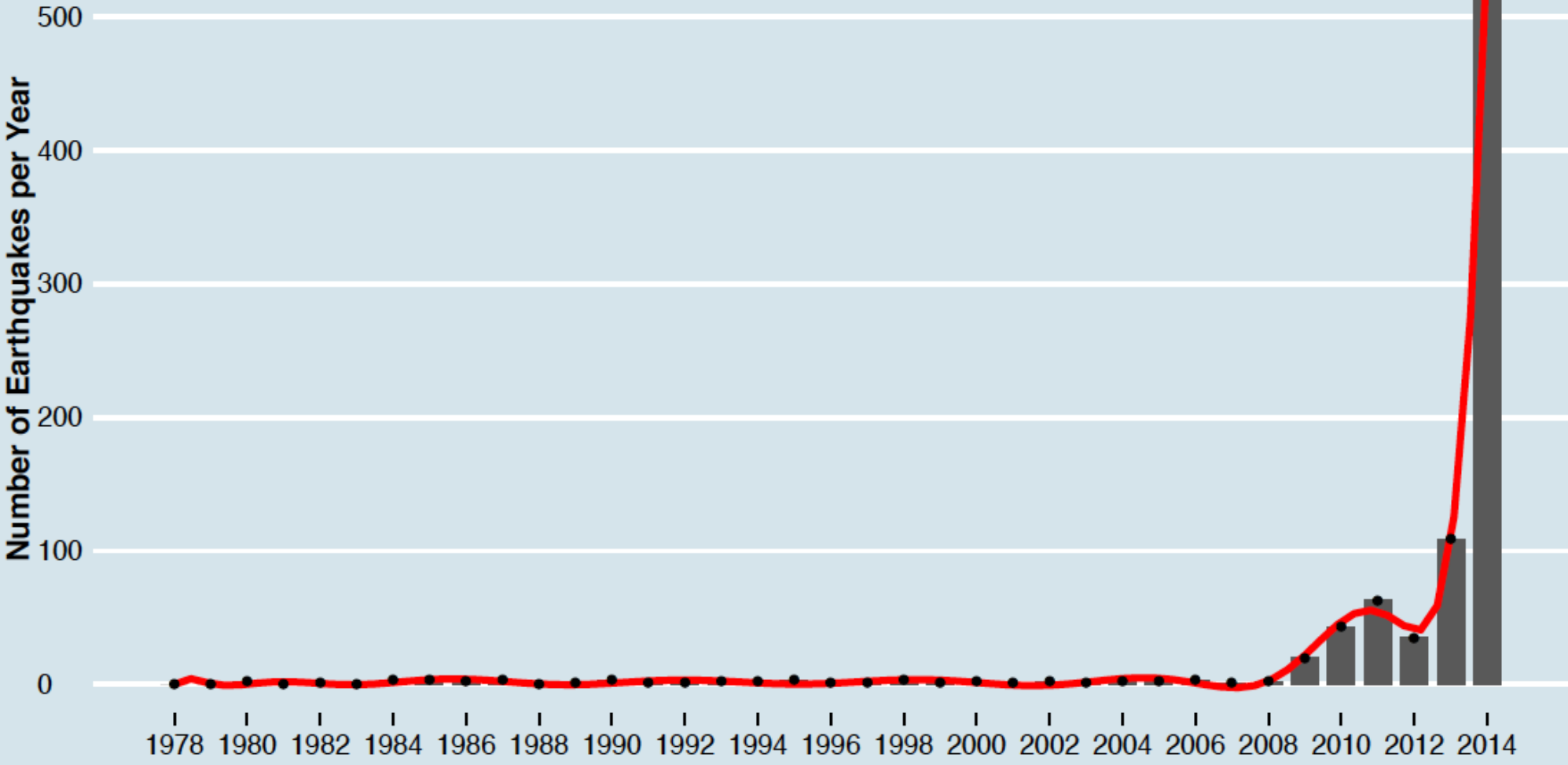


Figure modified from Walsh and Zoback, 2016

Oklahoma Earthquakes Magnitude 3.0 and greater



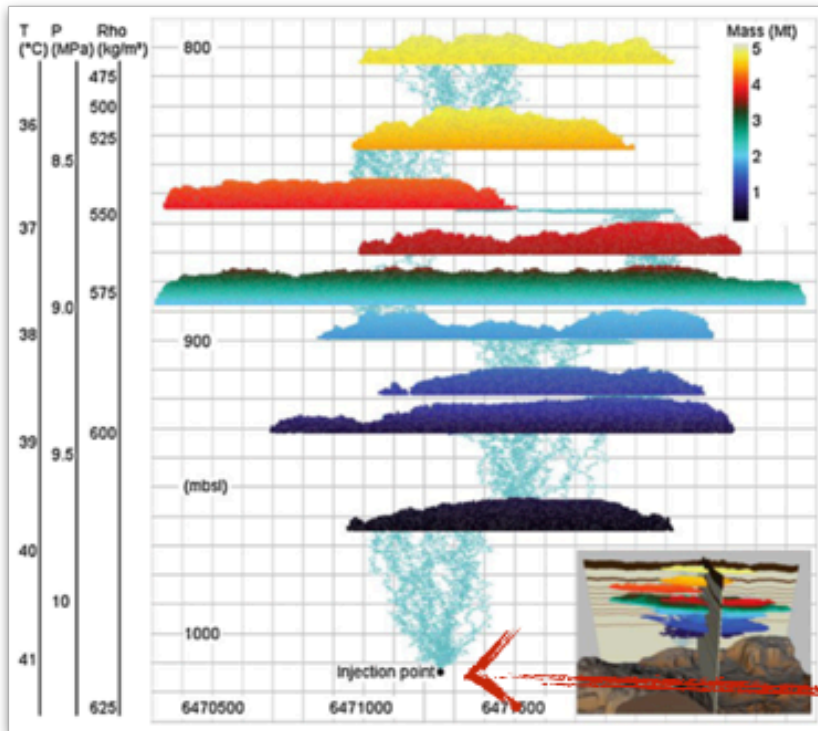
Fracture ~~or~~ and? flow?



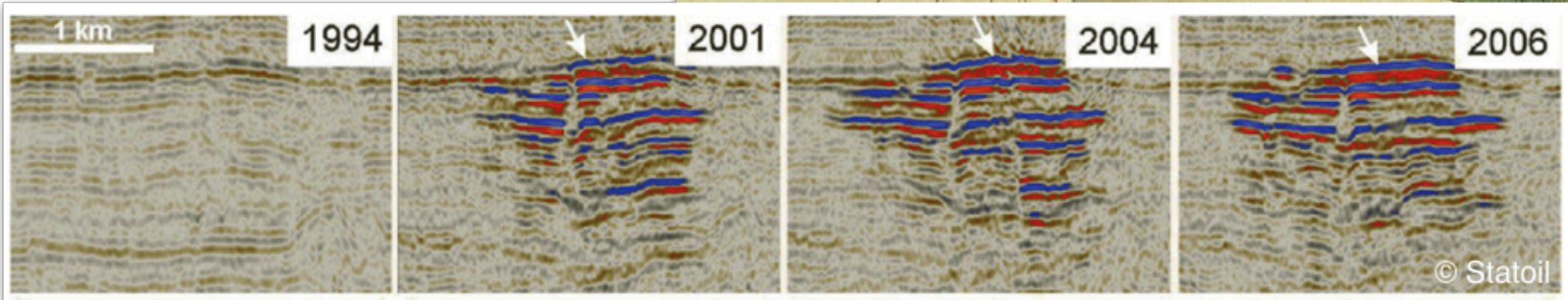
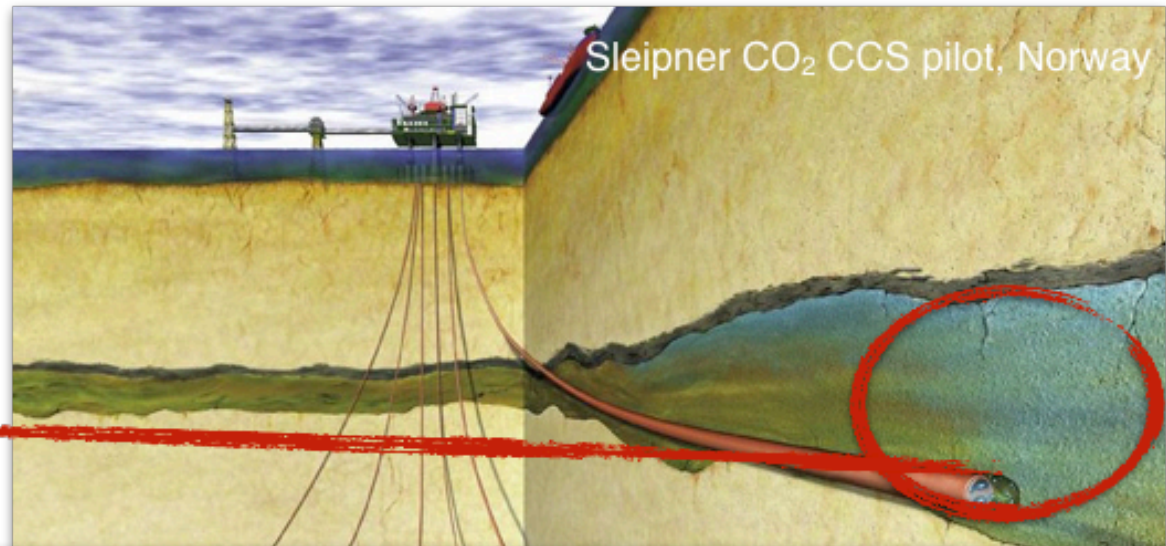
FLOW

Stability of a solid matrix
experiencing sustained flow

Sleipner gas field - the world's first offshore carbon capture and storage plant



Cavanagh and Haszeldine, 2014



Chadwick et al., 2009

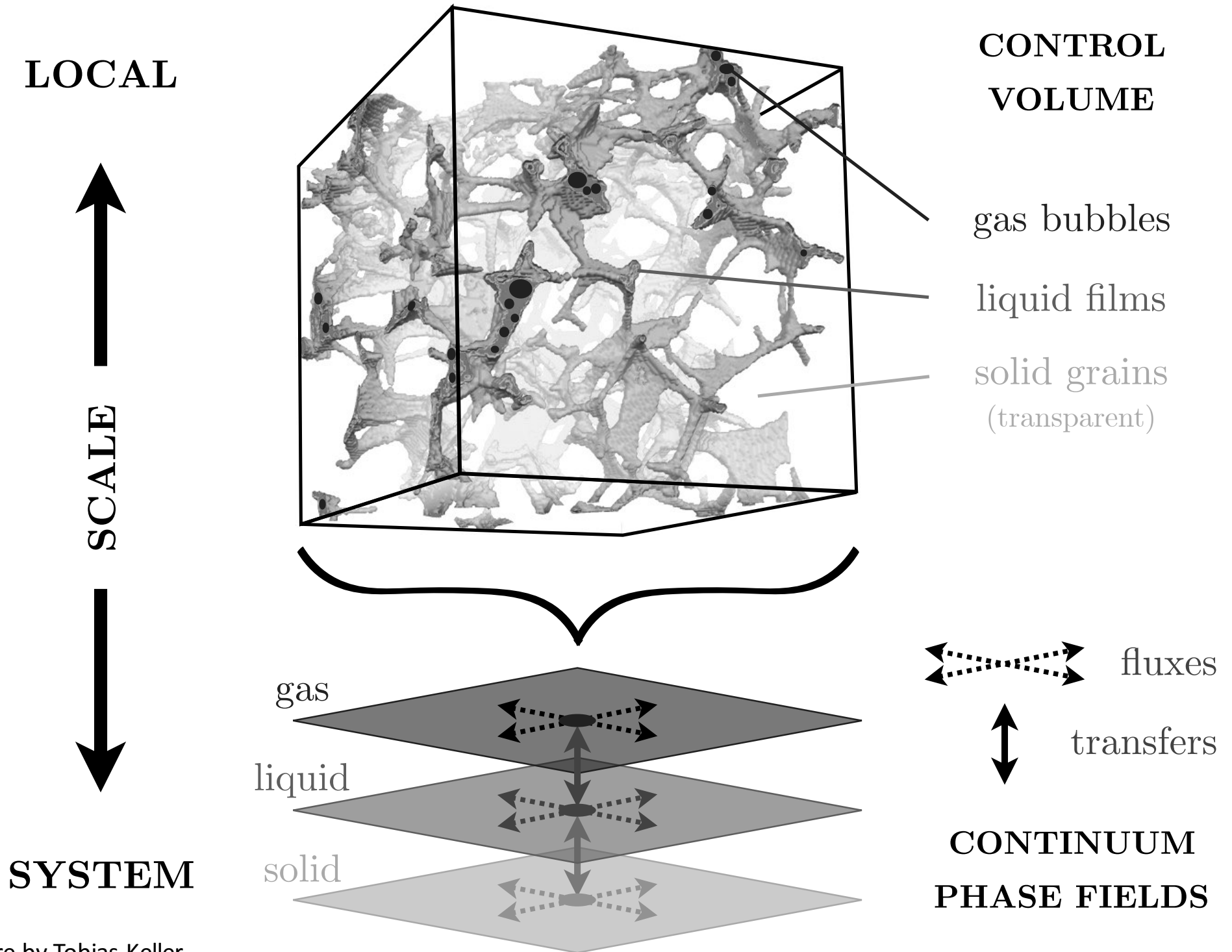


Figure by Tobias Keller



Tobias Keller

RATE OF CHANGE

DIFFUSIVE FLUX EXT SOURCE

$$\frac{\partial^i \phi^i \rho^i a^i}{\partial t} + \nabla \cdot \left(a^i \rho^i \mathbf{q}_\phi^i \right) + \nabla \cdot \mathbf{q}_a^i + \Gamma_a^i + Q_a^i = \Upsilon_a^i$$

MASS FLUX PHASE TRANSFER INT PRODUCTION

DIFFUSIVE FLUXES

\mathbf{q}_ϕ^i volume flux

\mathbf{q}_s^i entropy flux

$\underline{\mathbf{q}}_v^i$ momentum flux (stress)

\mathbf{q}_j^i chemical flux

PHASE TRANSFERS

Γ_ϕ^i volume transfer

Γ_s^i entropy transfer

$\vec{\Gamma}_v^i$ momentum transfer

Γ_j^i chemical transfer

EXT SOURCE

Q_ϕ^i none

Q_s^i radiogenic heating

\mathbf{Q}_v^i gravity body force

Q_j^i none

INT PRODUCTION

Υ_ϕ^i none

Υ_s^i entropy production

Υ_v^i none

Υ_j^i none

Multiphase mechanics



Tobias Keller

segregation velocity
 segregation coefficient
 pressure gradients
 viscous stress
 phase buoyancy

SEGREGATION $\mathbf{v}_{\Delta}^i = \phi^i \Delta \mathbf{v}^{i*} = - \frac{q_{\phi}^i}{\eta_{\phi}^i} \left(\phi^i \nabla P^* + \nabla P_{\Delta}^i - \nabla \cdot \phi^i \eta_{\phi}^i \mathbf{D}(\mathbf{v}^i) - \phi^i \rho^i \mathbf{g} \right)$

COMPACTION $P_{\Delta}^i = \phi^i \Delta P^{i*} = - \frac{\eta_{\phi}^i}{r_{\phi}^i} \left(\phi^i \nabla \cdot \mathbf{v}^* + \nabla \cdot \mathbf{v}_{\Delta}^i - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma^i}{\rho^i} \right)$

compaction pressure
 compaction coefficient
 velocity divergences
 phase compressibility
 mass transfer

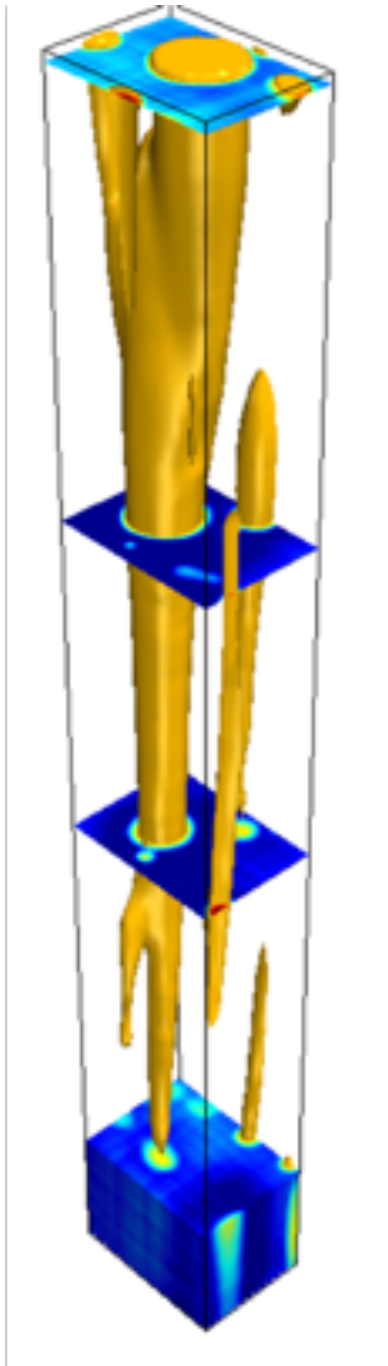


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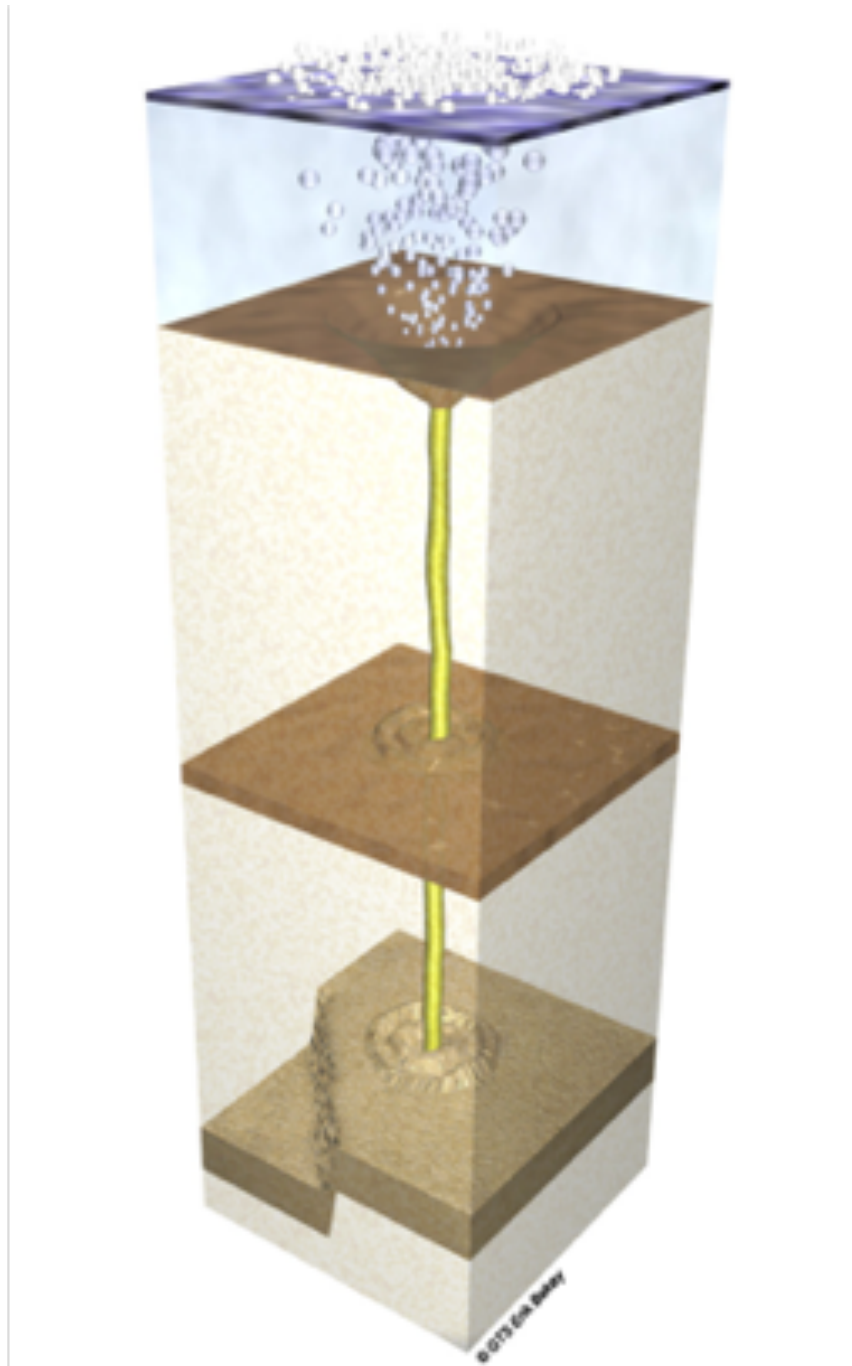
Multiphase mechanics

	segregation velocity	segregation coefficient	pressure gradients	viscous stress	phase buoyancy
SEGREGATION	$\boxed{\mathbf{v}_{\Delta}^i} = \phi^i \Delta \mathbf{v}^{i*} = - \frac{q_{\phi}^i}{\eta_{\phi}^i} \left(\phi^i \nabla P^* + \boxed{\nabla P_{\Delta}^i} - \nabla \cdot \phi^i \eta_{\phi}^i \mathbf{D}(\mathbf{v}^i) - \phi^i \rho^i \mathbf{g} \right)$				
COMPACTION	$\boxed{P_{\Delta}^i} = \phi^i \Delta P^{i*} = - \frac{\eta_{\phi}^i}{r_{\phi}^i} \left(\phi^i \nabla \cdot \mathbf{v}^* + \boxed{\nabla \cdot \mathbf{v}_{\Delta}^i} - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma^i}{\rho^i} \right)$				
	compaction pressure	compaction coefficient	velocity divergences	phase compressibility	mass transfer

Model

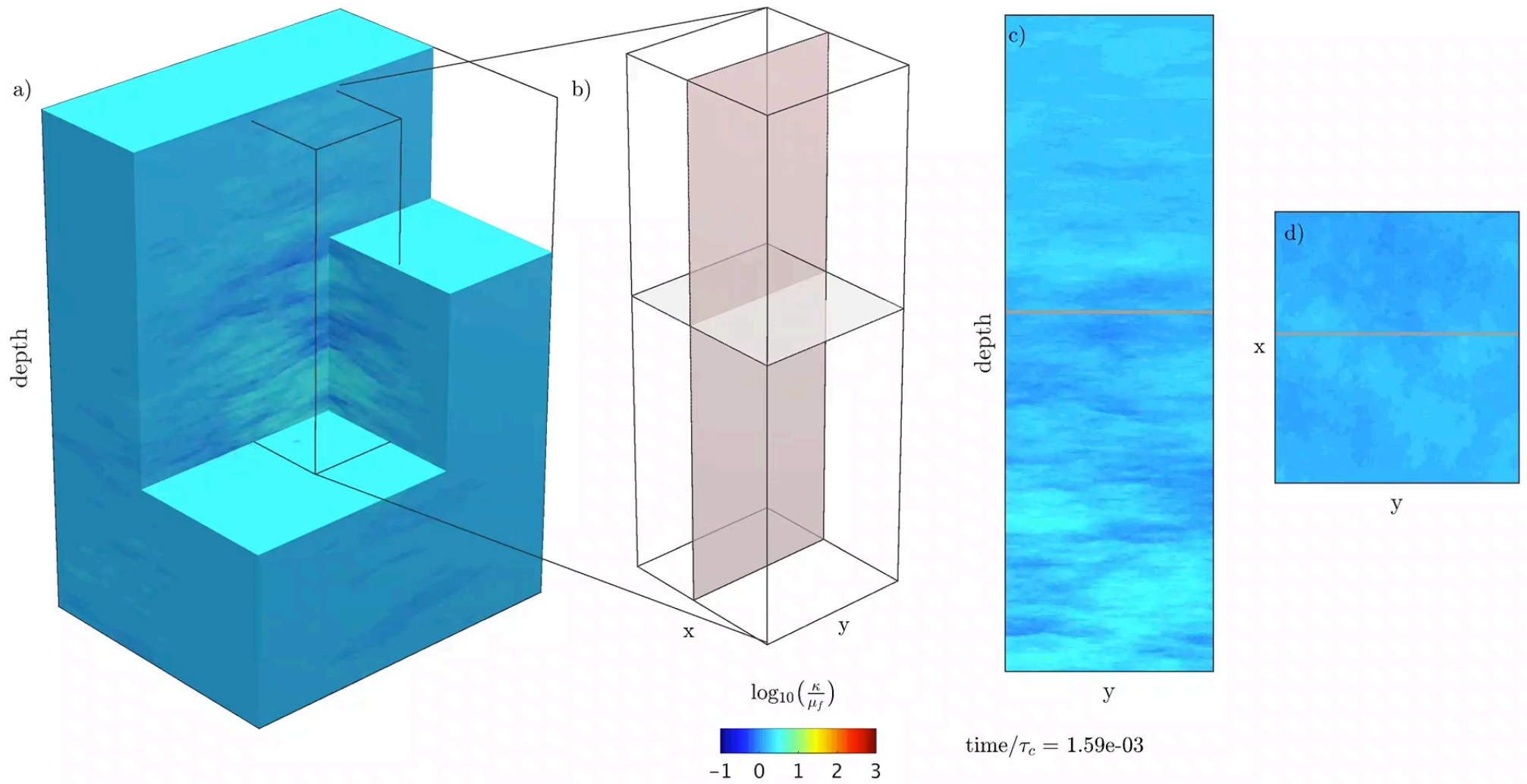


Observation



Ludovic Räss

3D GPU-based code by Ludovic Räss, see Räss et al., 2018, Sketch by Løseth et al, 2011



Simulations by Ludovic Räss, see Räss et al., 2018

Fracture ~~or~~ and? flow?

→ Sustained flow alters the structural integrity of a rock or granular matrix



FLOW

Stability of continuous rock experiencing sustained flow



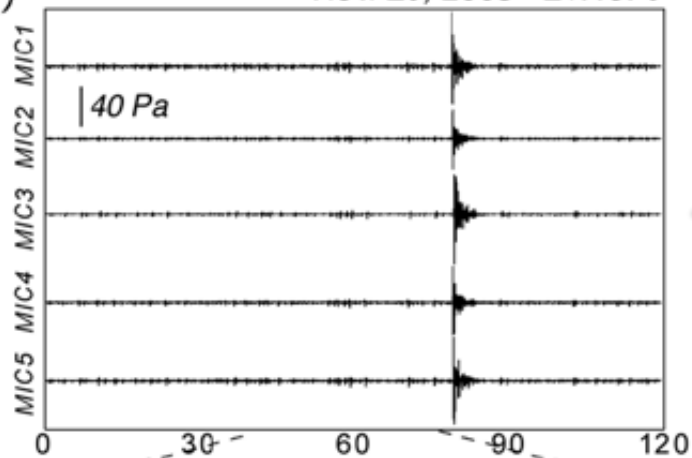
Figure by Google Earth Images



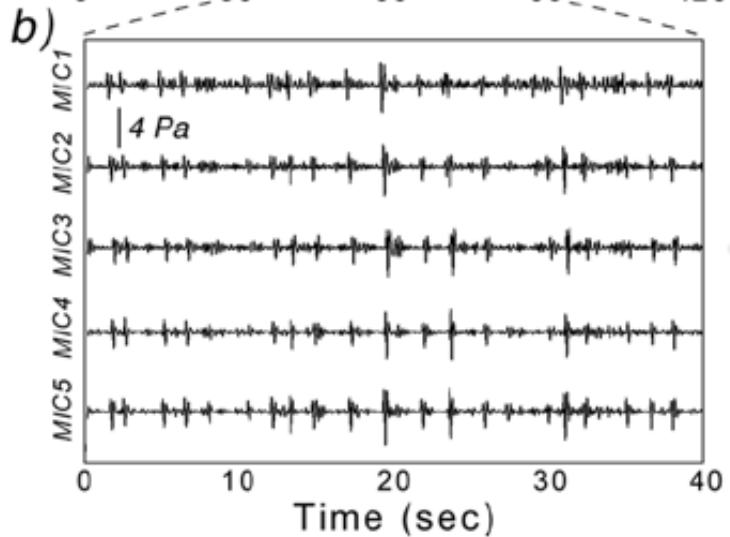
17:35:11



a) Nov. 20, 2003 - 21.15. 0

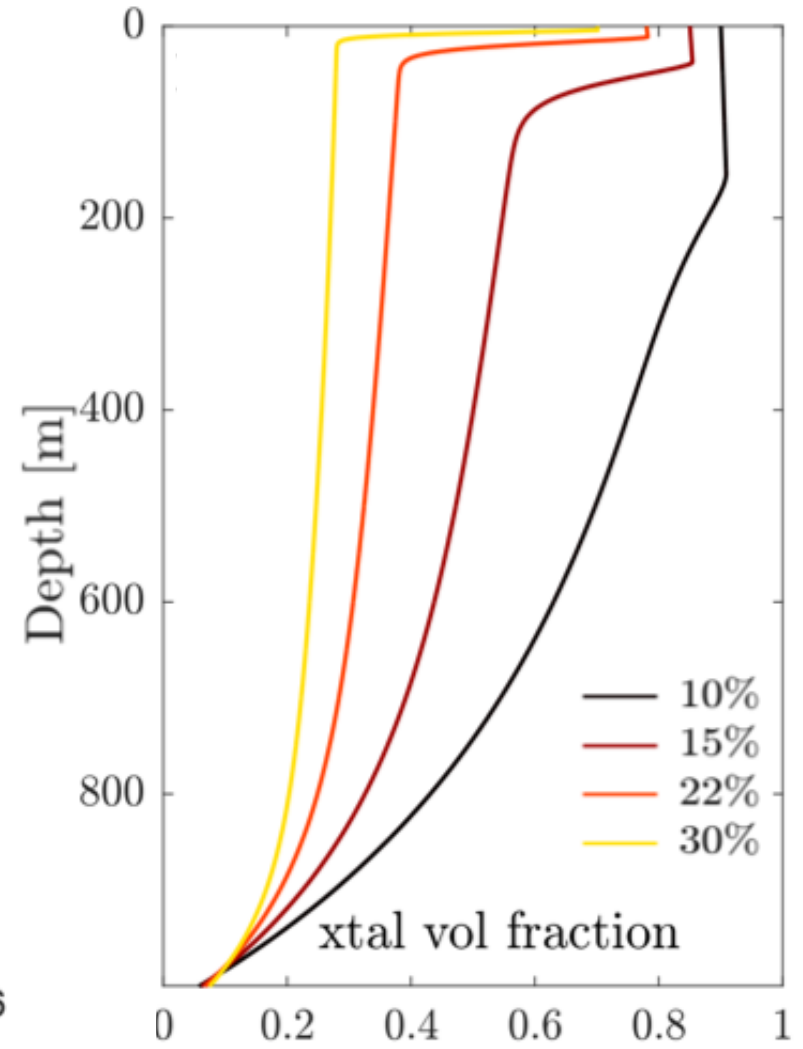
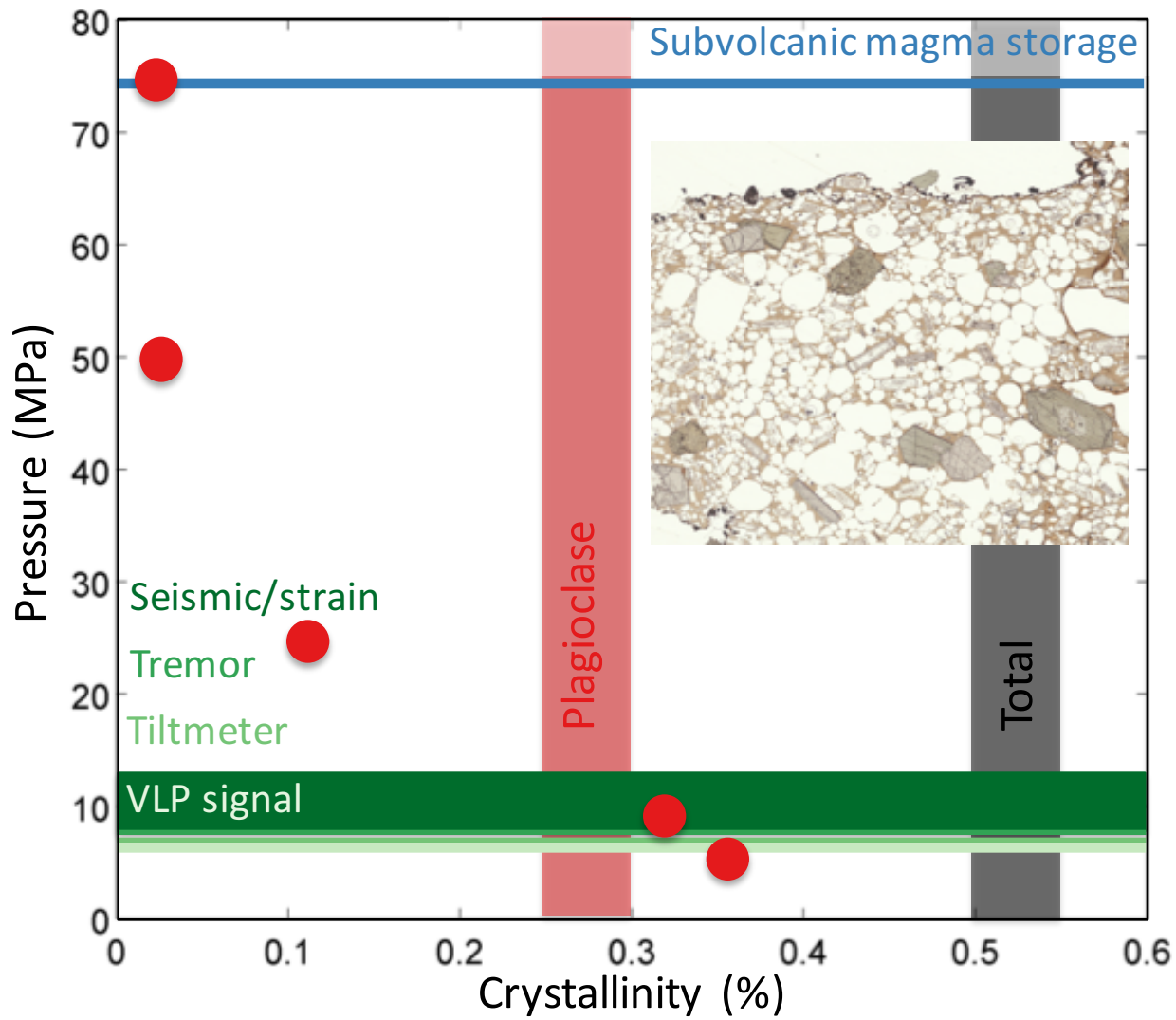


→ NORMAL STROMBOLIAN EXPLOSIONS: large infrasonic pulses ($>10\text{Pa}$) every 8-10 min

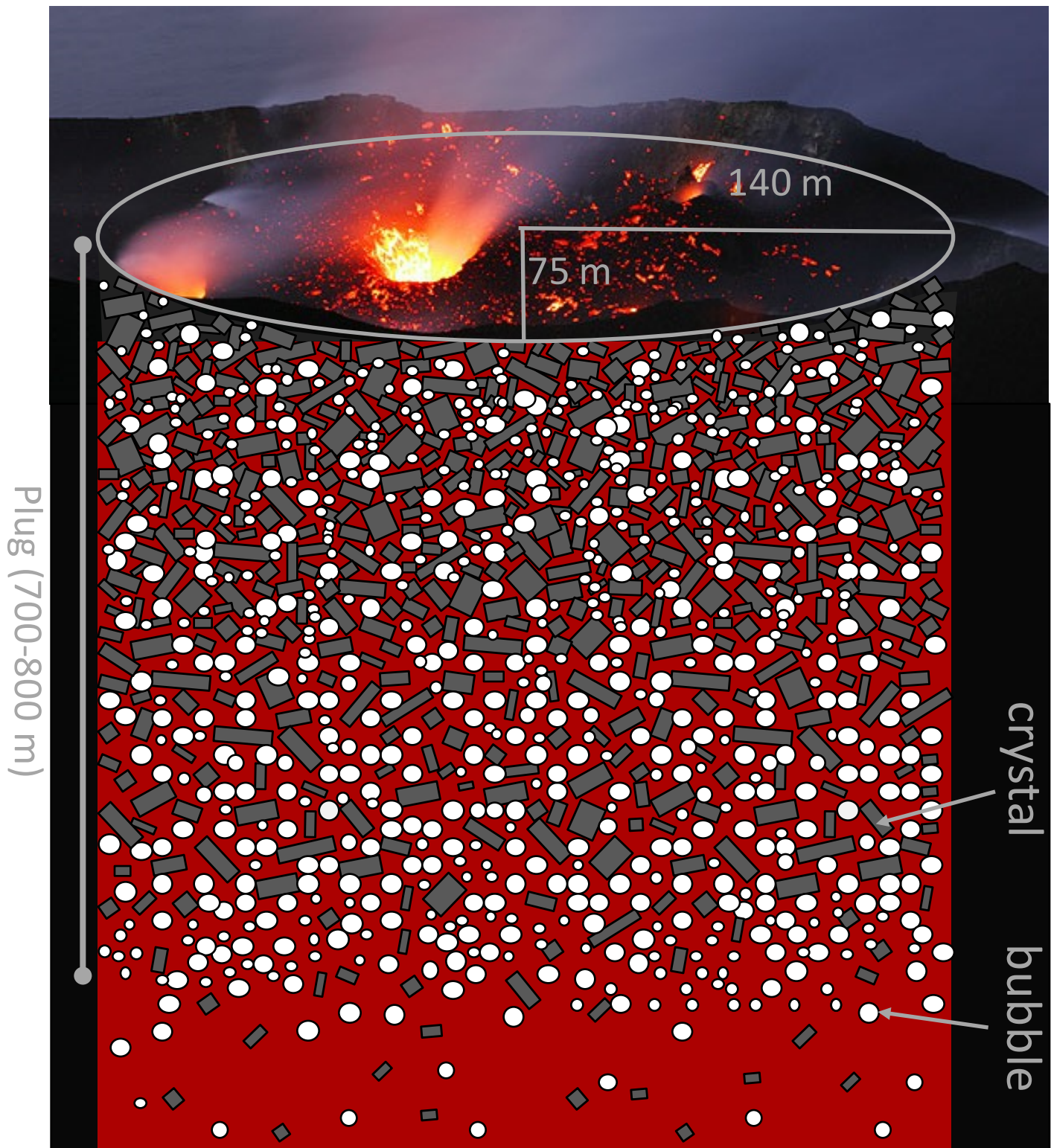


→ PUFFING: small infrasonic pulses ($\approx 1\text{Pa}$) every 1-2 s

PASSIVE DEGASSING: continuous and distributed



Experimental crystallinity data from Agostini et al. 2013; Computations from Suckale et al. 2016





Tobias Keller

Governing equations

SEGREGATION

conservation of phase momentum

$$\phi^i \Delta \mathbf{v}^{i*} = -\frac{q_\phi^i}{\eta_\phi^i} \left(\phi^i \nabla P^* + \nabla \phi^i \Delta P^{i*} - \nabla \cdot \phi^i \eta_\phi^i \mathbf{D}(\mathbf{v}^i) - \phi^i \rho^i \mathbf{g} \right)$$

COMPACTION

conservation of phase mass

$$\phi^i \Delta P^{i*} = -\frac{\eta_\phi^i}{r_\phi^i} \left(\phi^i \nabla \cdot \mathbf{v}^* + \nabla \cdot \phi^i \Delta \mathbf{v}^{i*} - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma_\rho^i}{\rho^i} \right)$$

PHASE EVOLUTION

conservation of phase volume

$$\frac{D^i \phi^i}{Dt} = \nabla \cdot \kappa_\phi^i \nabla \Delta \phi^{i*} - \phi^i \nabla \cdot \mathbf{v}^i - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma_\rho^i}{\rho^i}$$

CHEMICAL EVOLUTION

conservation of component mass

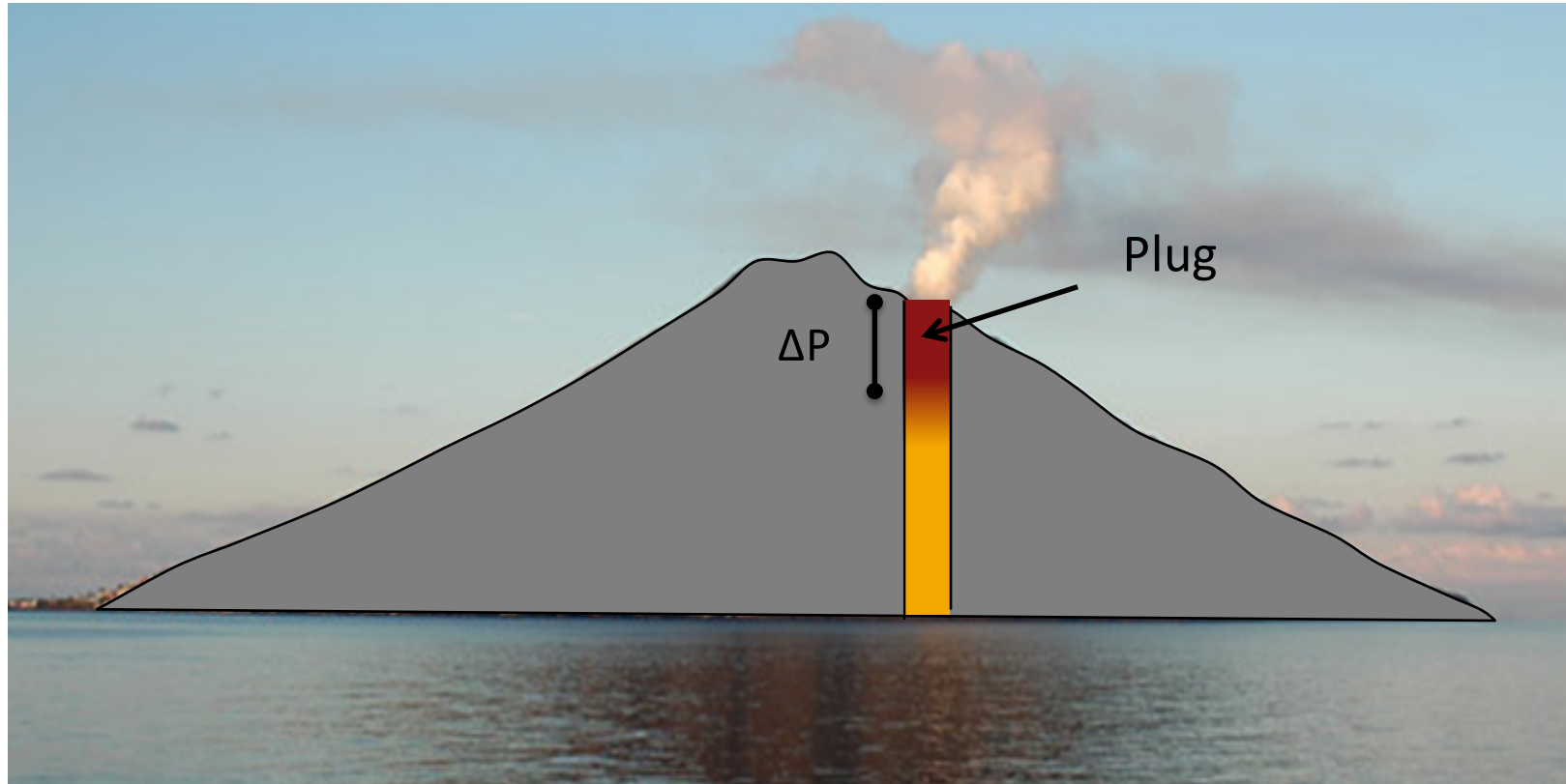
$$\frac{D^i c_j^i}{Dt} = \nabla \cdot \kappa_j^i \nabla \Delta c_{j*}^i + \frac{\Delta c_j^{i\Gamma} \Gamma_\rho^i}{\phi^i \rho^i}$$

THERMAL EVOLUTION

conservation of phase energy

$$\frac{D^i T^i}{Dt} = \nabla \cdot \kappa_T^i \nabla T^i - \frac{\kappa_T^i}{d^{i2}} \Delta T^{i*} + \frac{L^{i*} \Gamma_\rho^i}{\phi^i \rho^i c_p^i} + \frac{\Psi^i}{\phi^i \rho^i c_p^i} + \frac{\alpha^i T^i}{\rho^i c_p^i} \frac{D^i P^i}{Dt} + \frac{H^i}{c_p^i}$$

Regime 1: Darcy flow



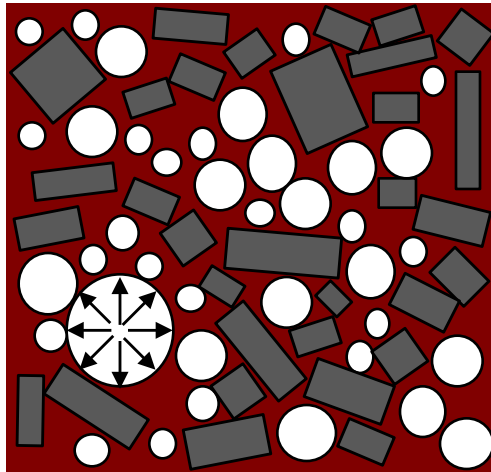
$u_m \ll u_g$ \longrightarrow No overpressure

$$q_g = -\frac{k(T)}{\mu_g} \nabla P$$

Regime 2: Degassing waves

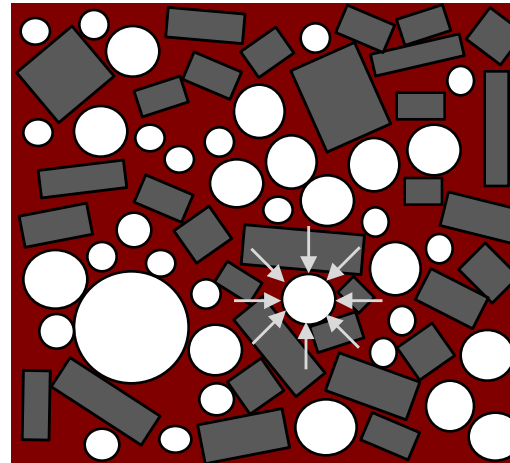
➔ $\lambda \approx 1 - 10\text{m}$

Gas expansion

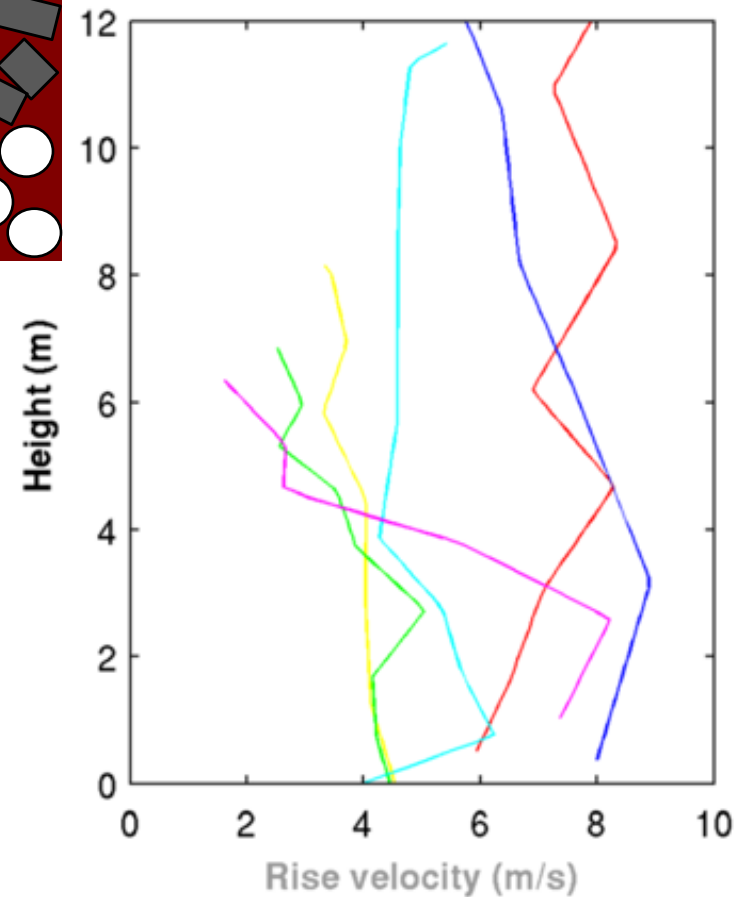


VS

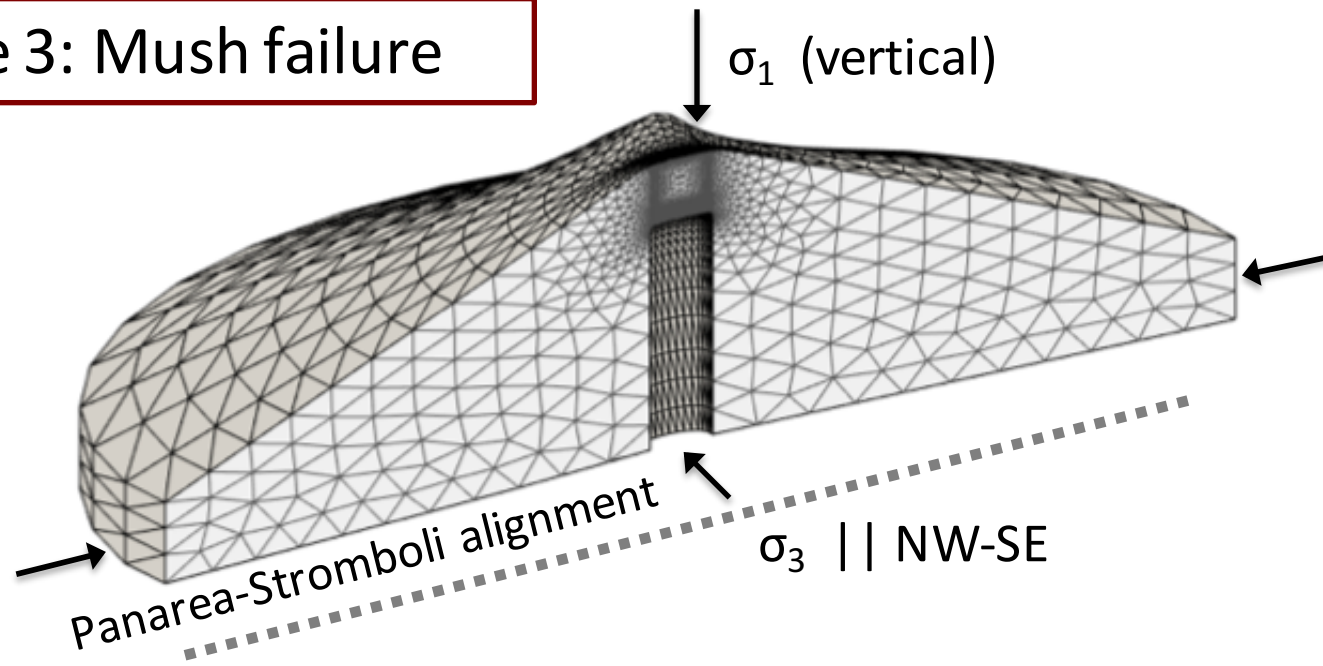
Magma creep



➔ Pressure pulses every 1-2s

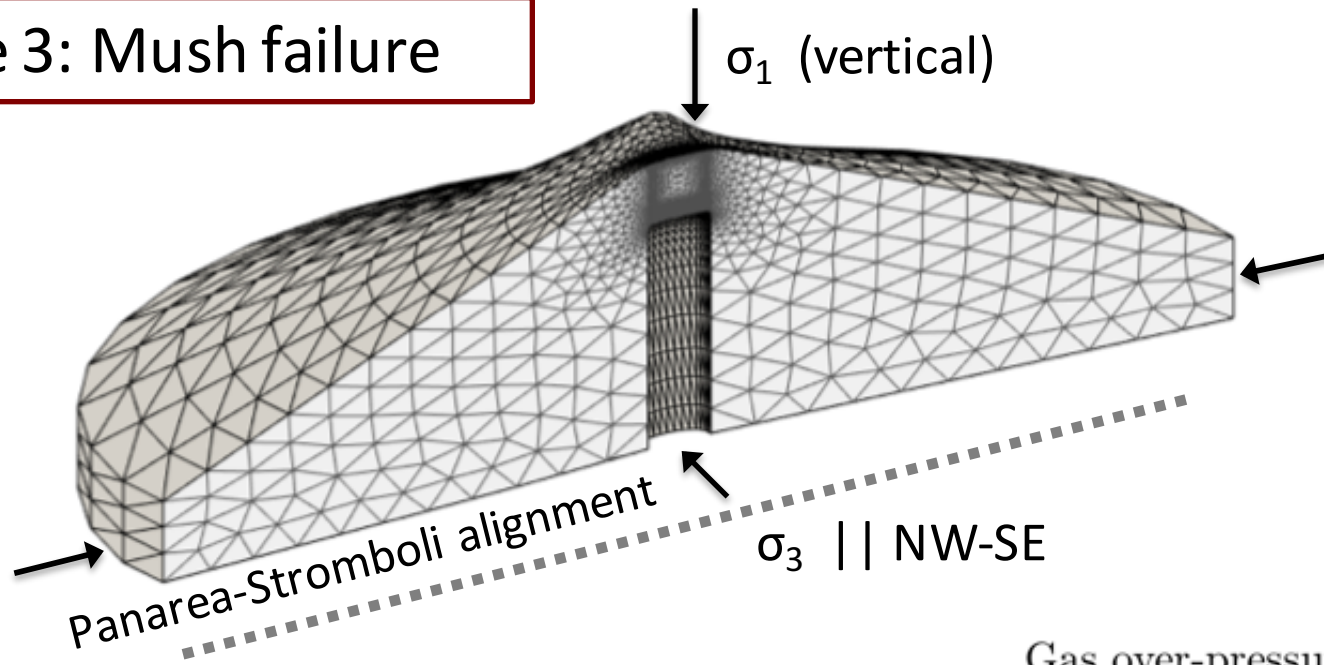


Regime 3: Mush failure



$$\tau_* = f(\sigma_n - p)$$

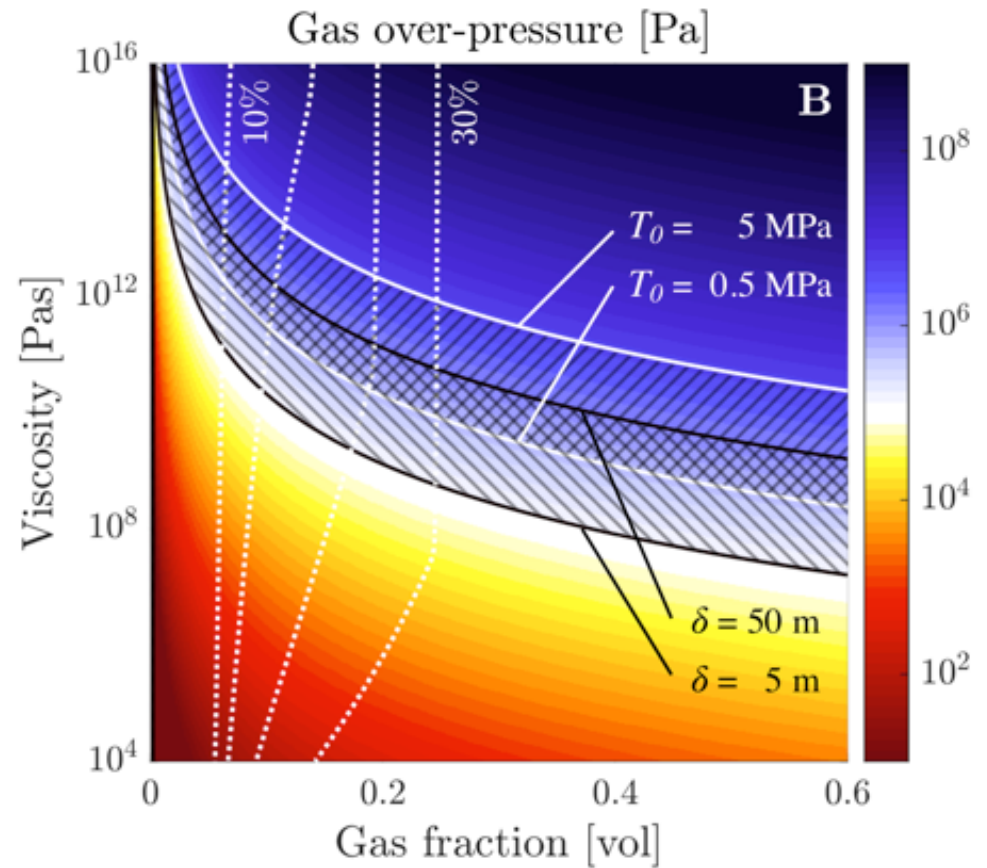
Regime 3: Mush failure

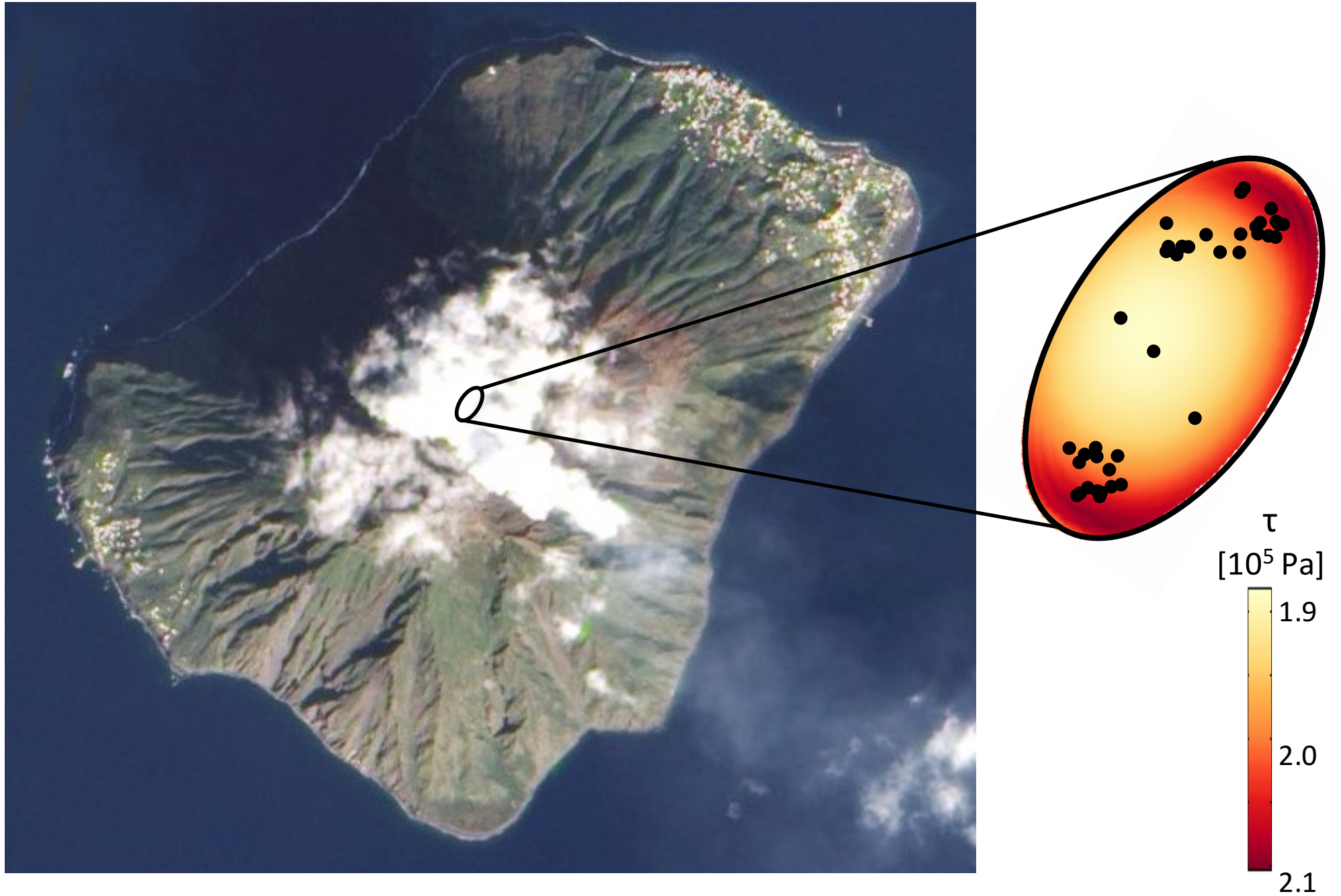


$$\tau_* = f(\sigma_n - p)$$

$$p_c := p_g - p_m = \zeta \nabla \cdot \mathbf{v}_m$$

$$\sim \Delta \rho g \delta$$



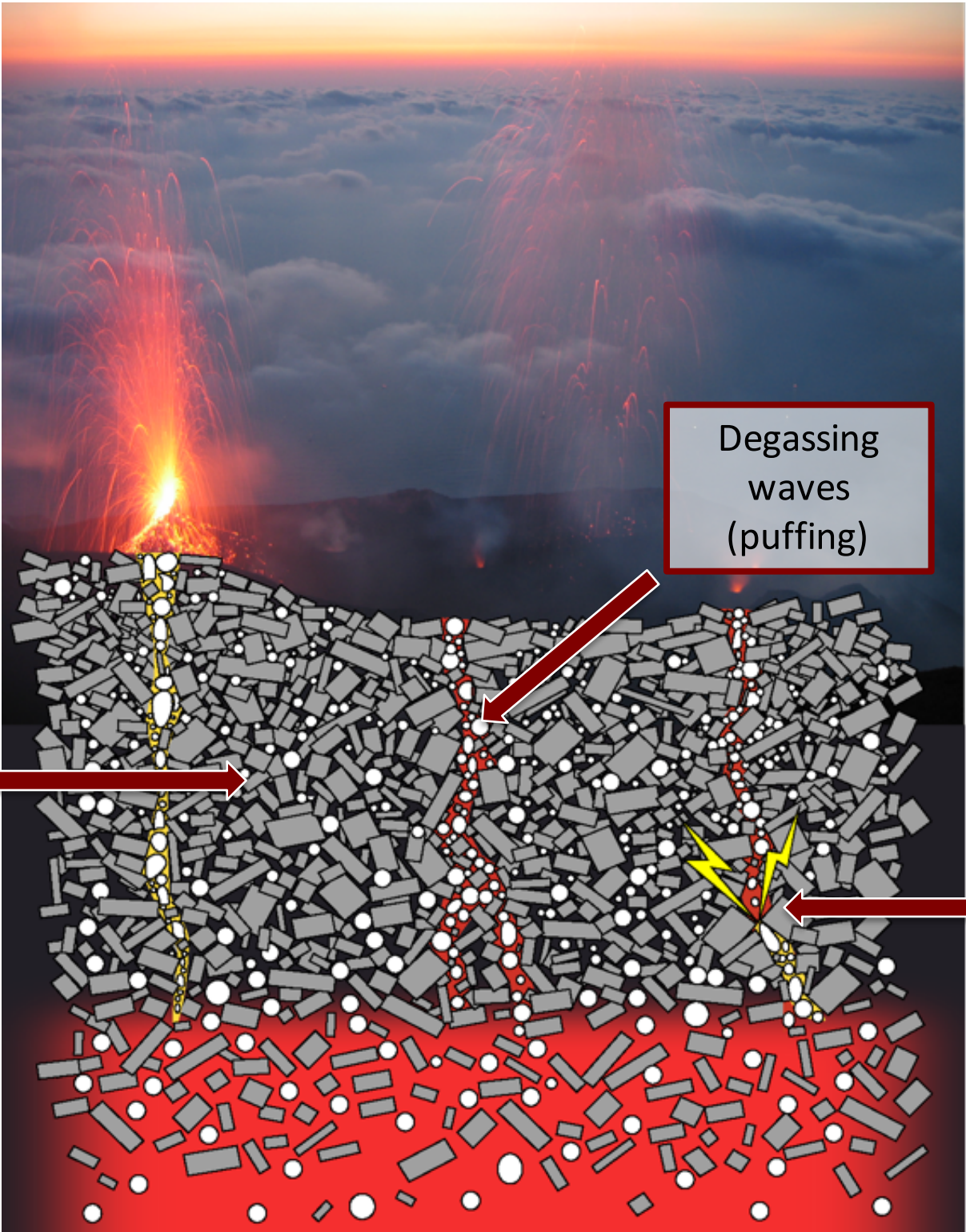


NASA ISS Image: Stromboli Volcano, Italy; Crater locations from Harris et al. 1996; Suckale et al. 2016

Darcy flow
(passive
degassing)

Degassing
waves
(puffing)

Mush failure
(normal
explosions)



Fracture ~~or~~ and? flow?

→ Sustained flow alters the structural integrity of a rock or granular matrix

→ The interplay between flow and matrix deformation results in overpressure and may entail failure



FLOW

Stability of continuous rock experiencing sustained flow



ICE



FIRE



ROCK



WATER

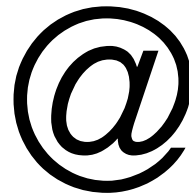
Conclusions:

- 1) Multiphase interactions at the granular scale can trigger a shift in the system-scale dynamics.
- 2) Fracture and flow often occur simultaneously and interact more dynamically than we usually give them credit for.
- 3) Studying extreme events across different natural systems with a similar model increases opportunities to refute/validate models.

Thank you.

Look deep into nature and you will understand everything better.

– Albert Einstein



GitLab



ICME



Minamisanriku, Japan:
95 % buildings destroyed
60% population missing
40% evacuation sites flooded



100 out of 300 km of sea walls in Tohoku destroyed.



Tohoku in dark green, source: Wiki

Bottom: Arahama, Miyagi Prefecture; Top: Yamada, Iwate Prefecture



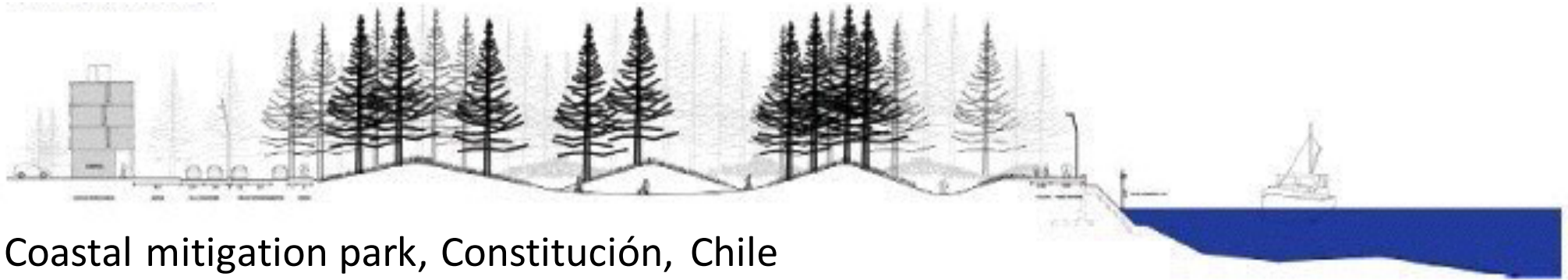
A photograph of a man in a white t-shirt, white pants, and green rubber boots standing on a concrete pier. He is holding a long, thin bamboo pole vertically against the wall. The background shows a blue sea with rocky islands under a blue sky with scattered white clouds. The text '\$6, 800, 000, 000' is overlaid in the center of the image.

\$6, 800, 000, 000

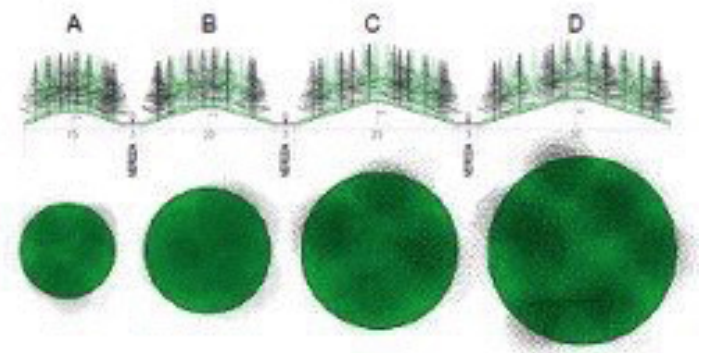
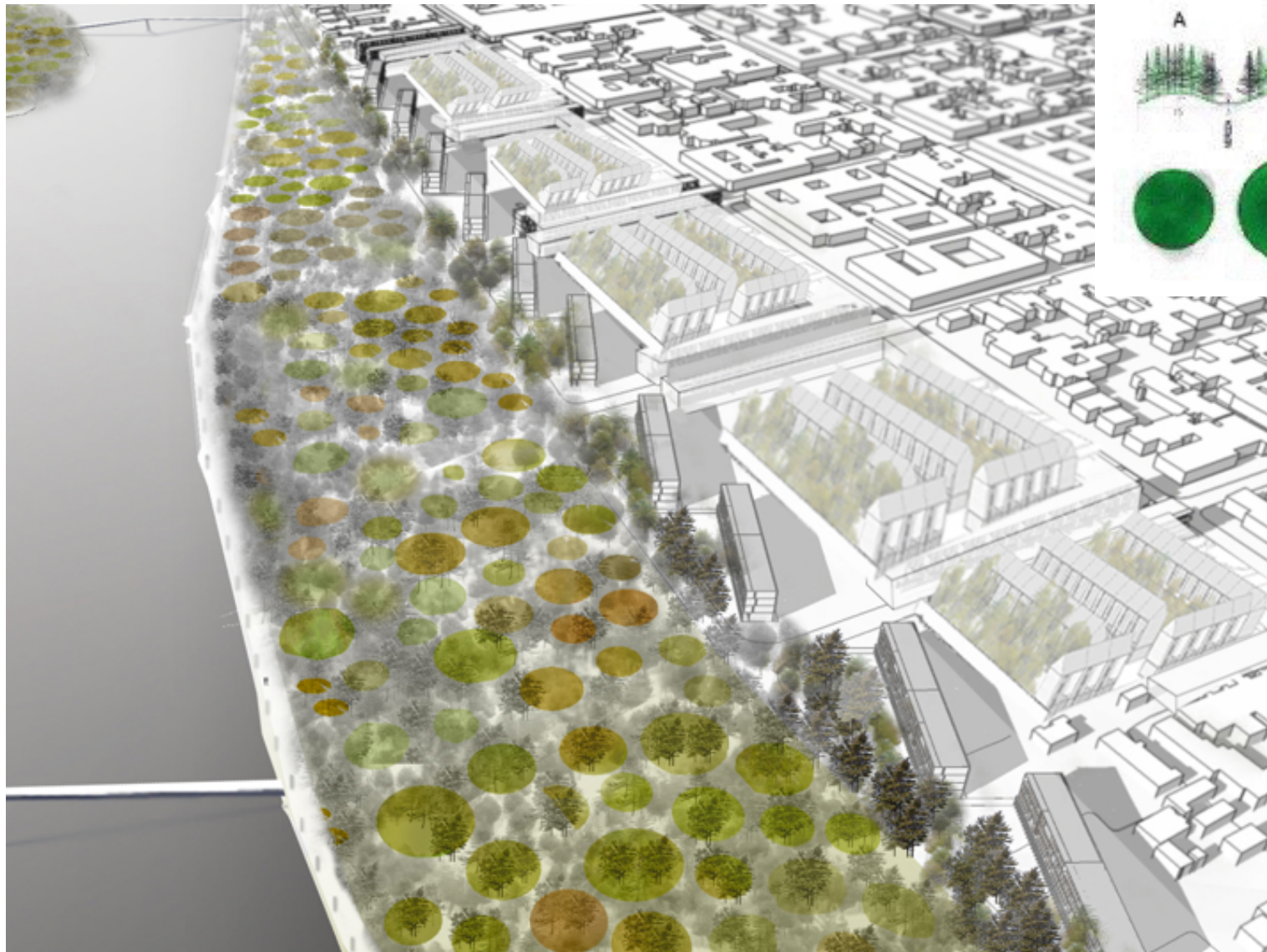


70 000 pine trees in Rikuzentakata destroyed, except for one “miracle pine”.





Coastal mitigation park, Constitución, Chile



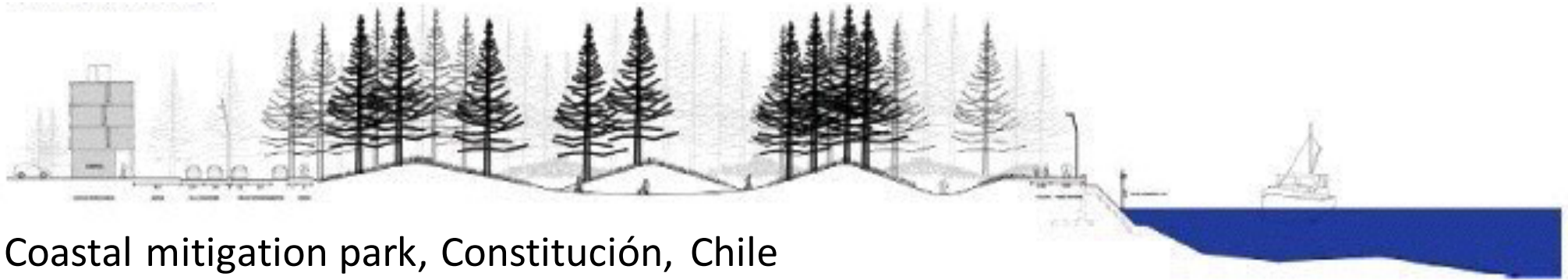
Hill sizes:

A: 2.0 x 15m

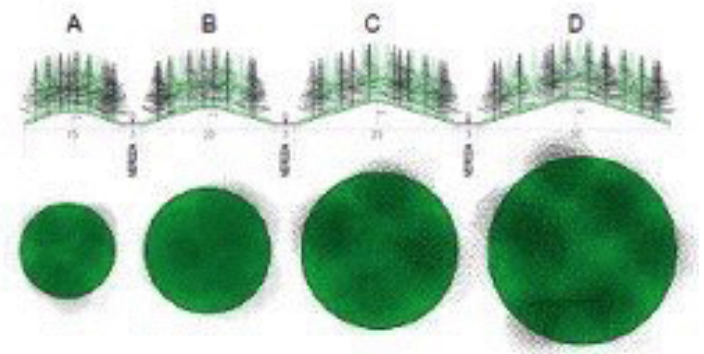
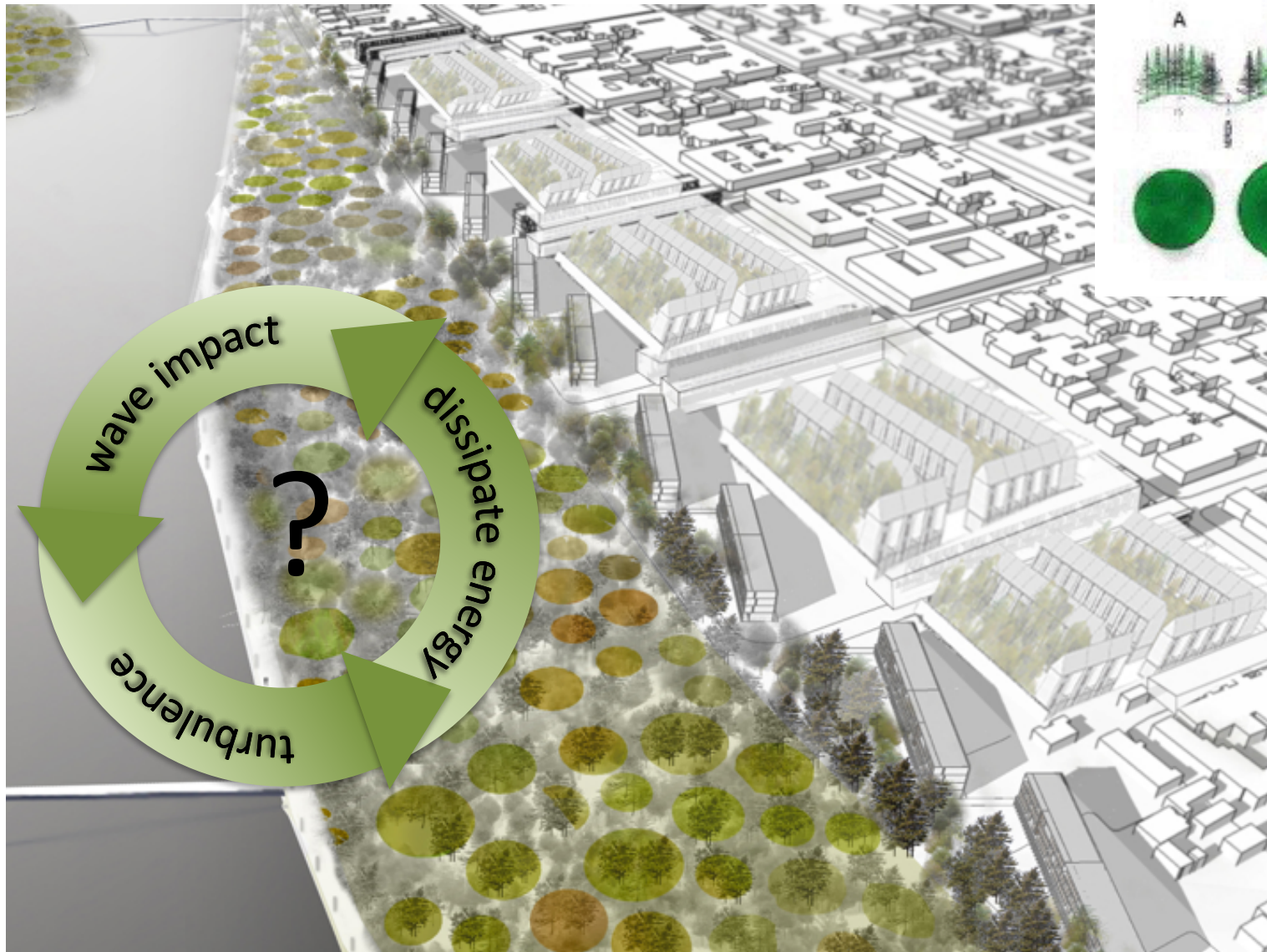
B: 2.6 x 20m

C: 3.4 x 25m

D: 4.0 x 30m



Coastal mitigation park, Constitución, Chile



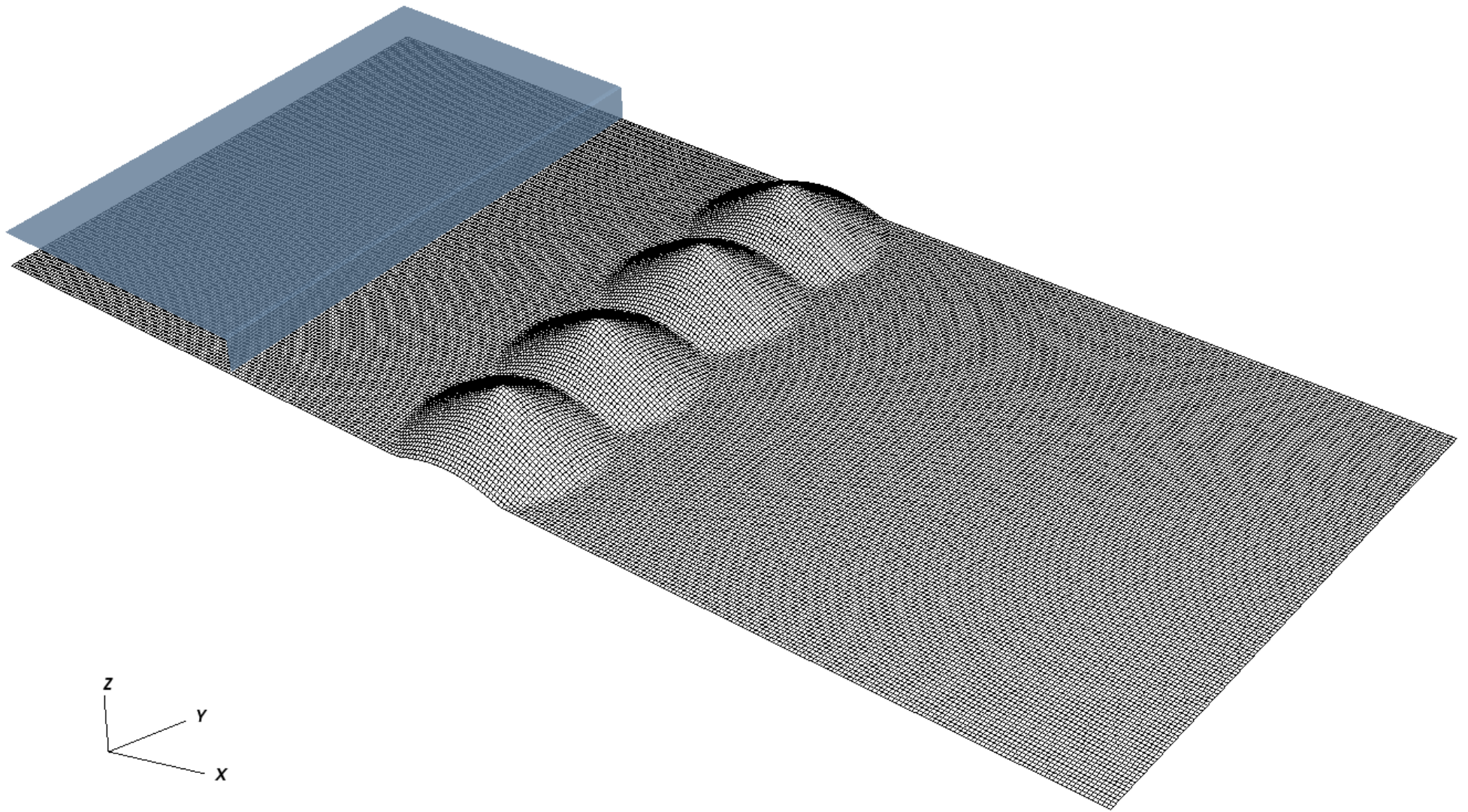
Hill sizes:

A: 2.0 x 15m

B: 2.6 x 20m

C: 3.4 x 25m

D: 4.0 x 30m



Viscous shallow water equations (NUMA2D)

Continuity:
$$\frac{\partial h}{\partial t} + \nabla \cdot (h\mathbf{u}) = \delta \nabla \cdot (\mu_{SGS} \nabla h)$$

↑
Switches viscosity on/off

Momentum:

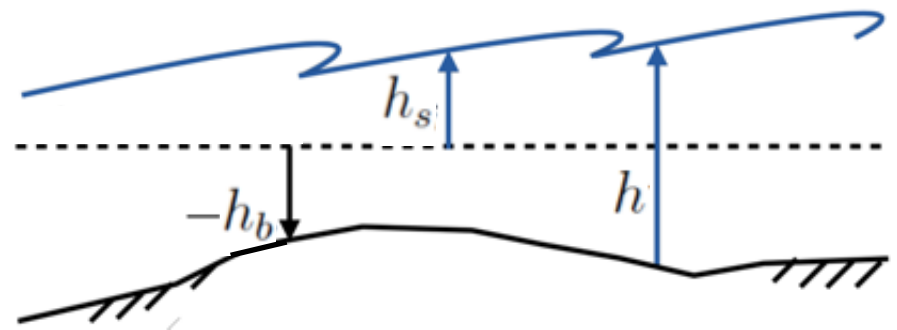
$$\frac{\partial h\mathbf{u}}{\partial t} + \nabla \cdot \left(h\mathbf{u} \otimes \mathbf{u} + \frac{g}{2}(h^2 - h_b^2)I \right) + gh_s \nabla \cdot (h_b I) = \nabla \cdot (h_s \mu_{SGS} \nabla \mathbf{u})$$

↑ ↑ ↑
Bathymetry Free surface Dynamic dissipation

Dynamic dissipation coefficient:

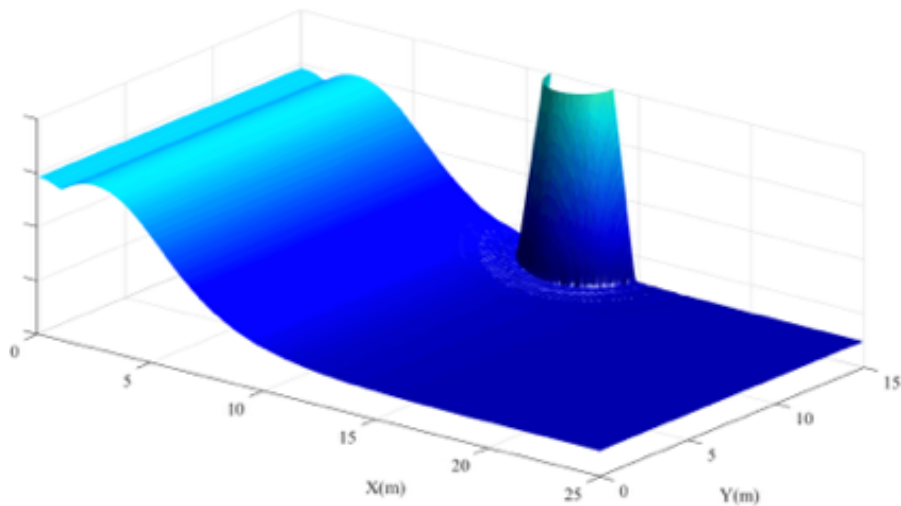
$$\mu_{SGS} = \max(0, \min(\mu_{\max}, \mu_{\text{res}}))$$

Wetting&drying: 0.1 m threshold

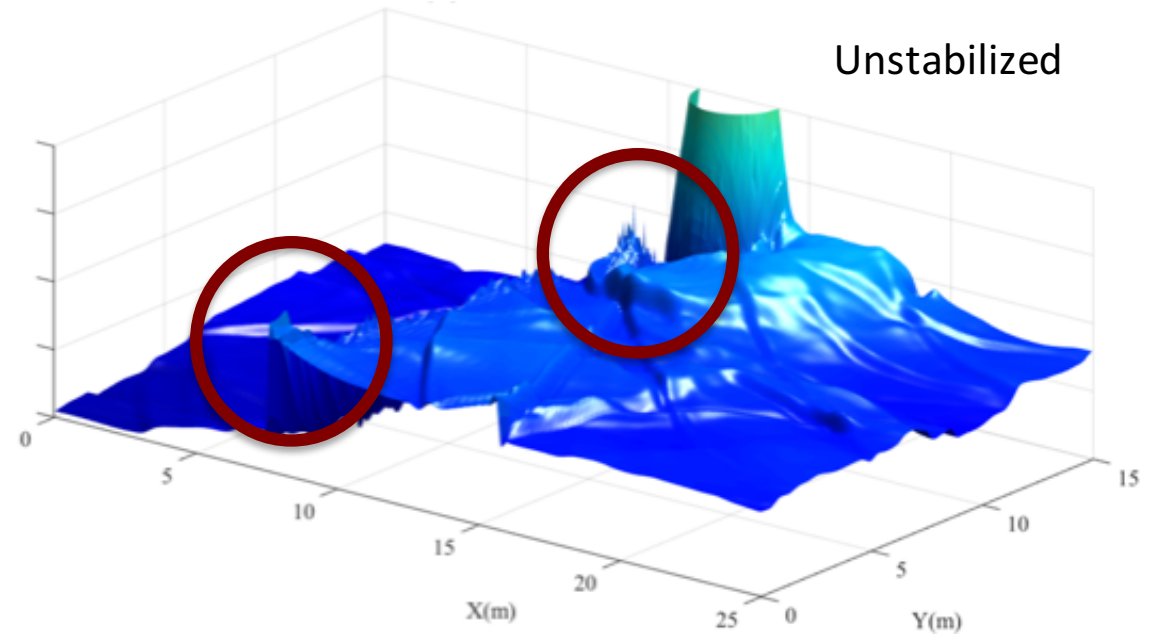


2D solitary wave runup on circular island

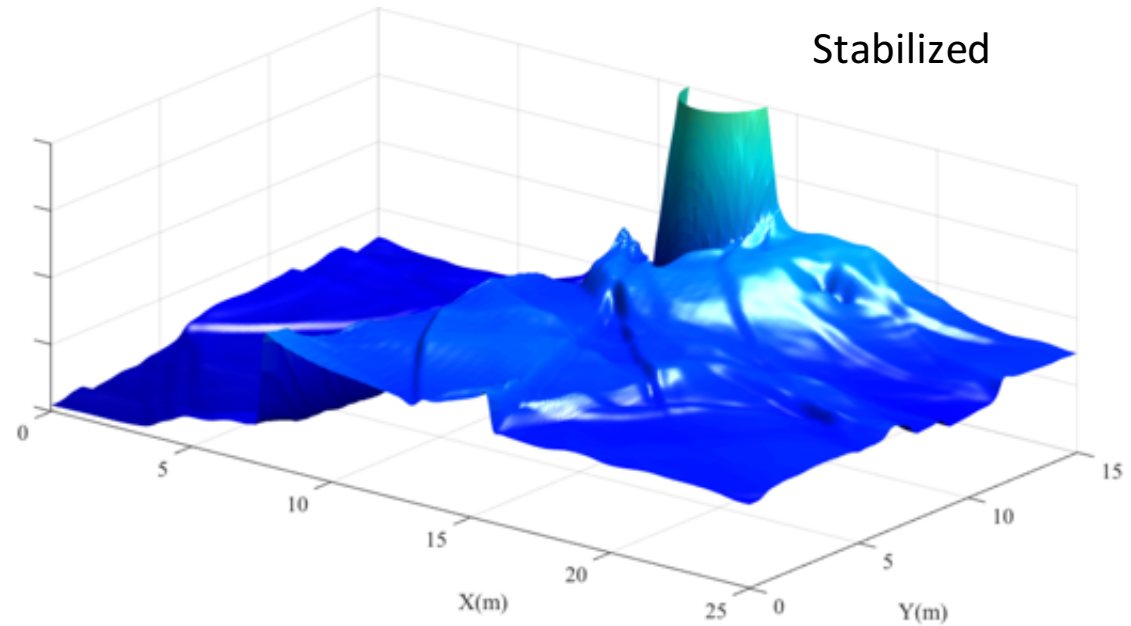
Initial condition



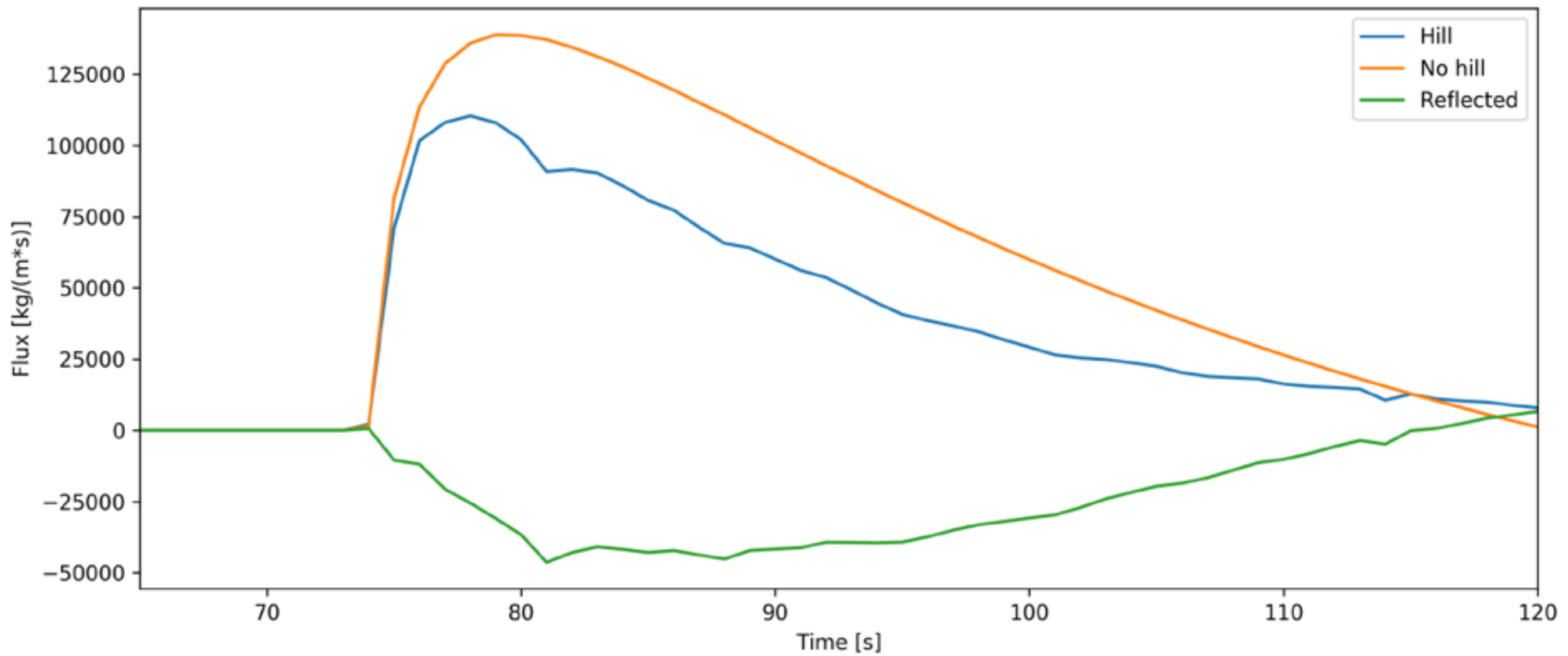
Unstabilized



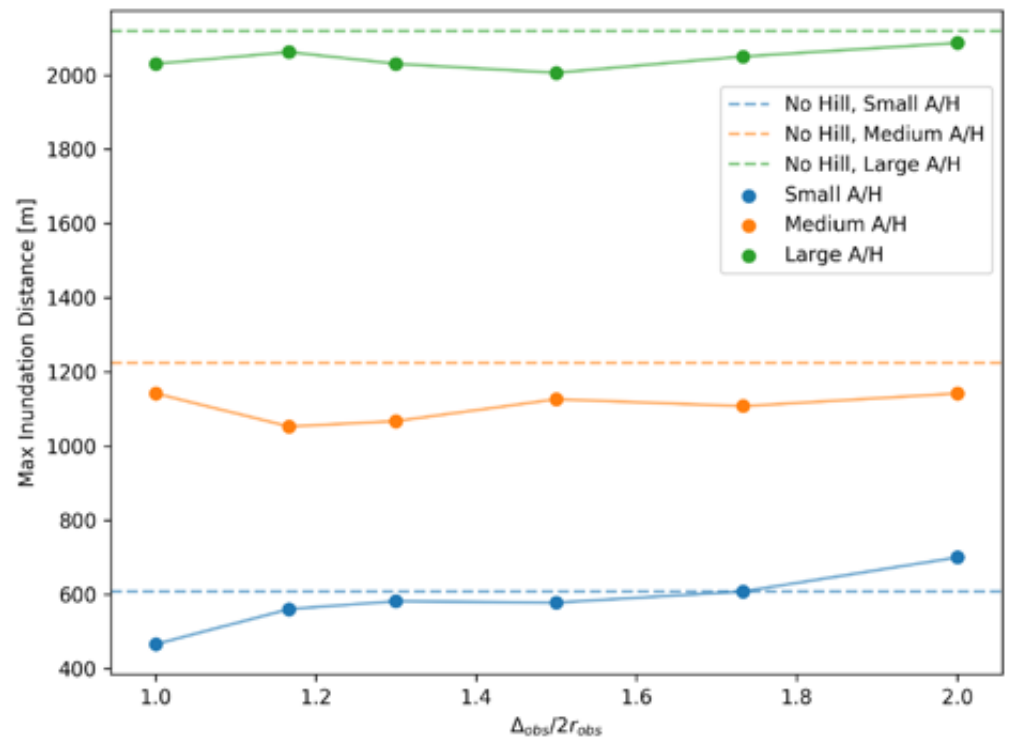
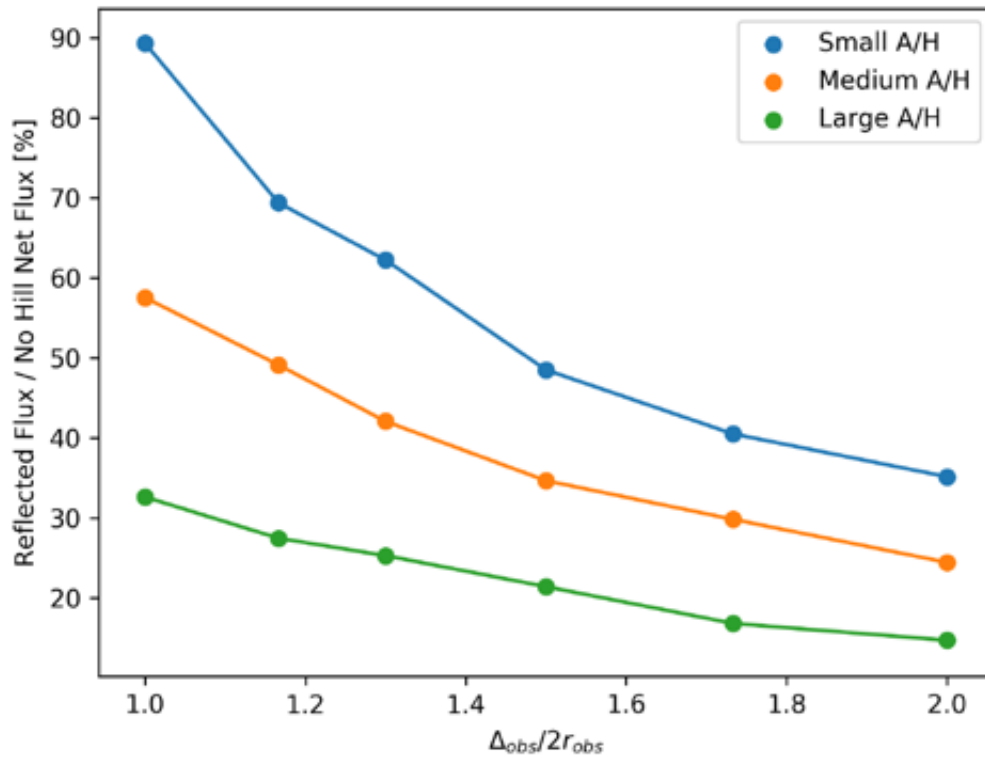
Stabilized

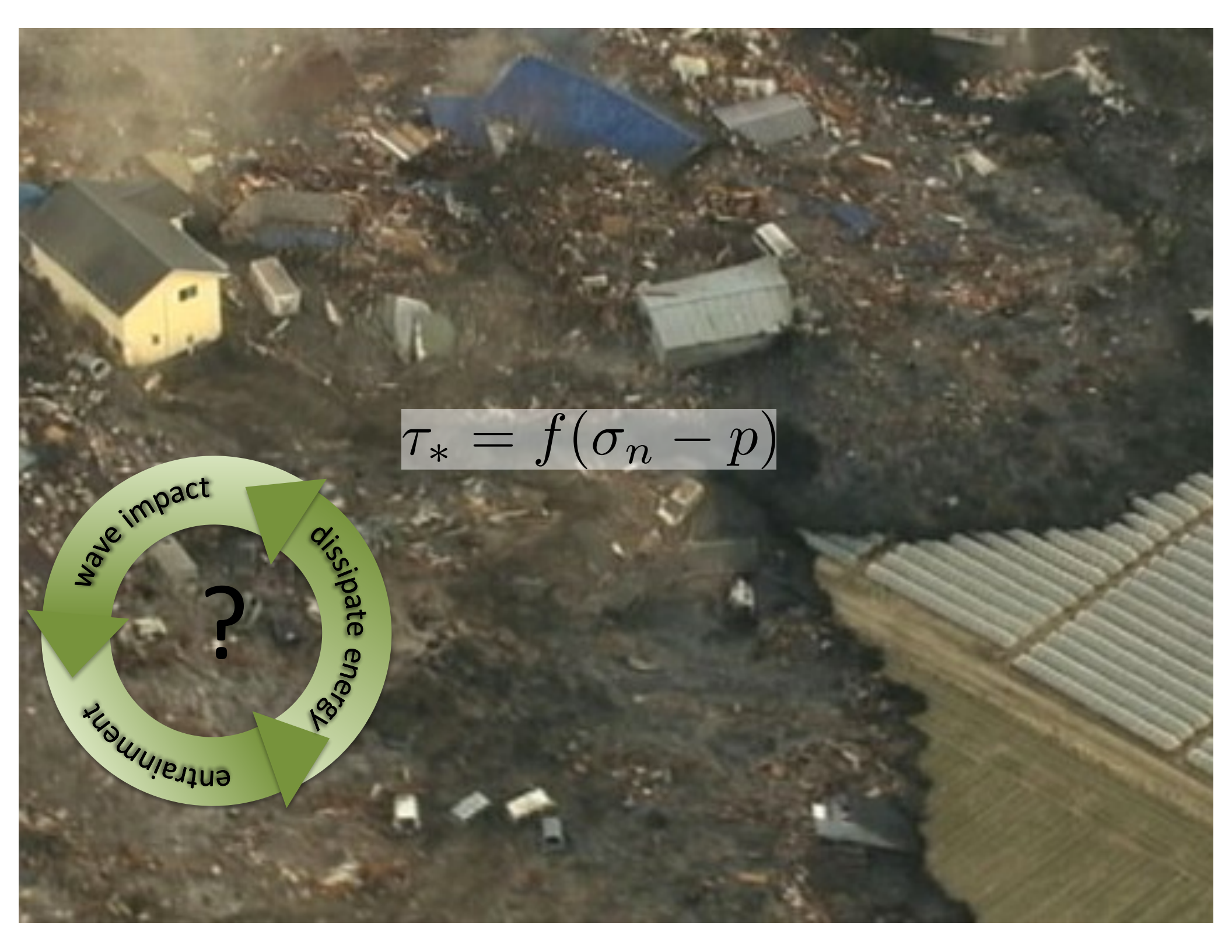


$$F = \int_0^{y_{\max}} \rho u(x = x_{\text{obs}}) \cdot h \, dy$$



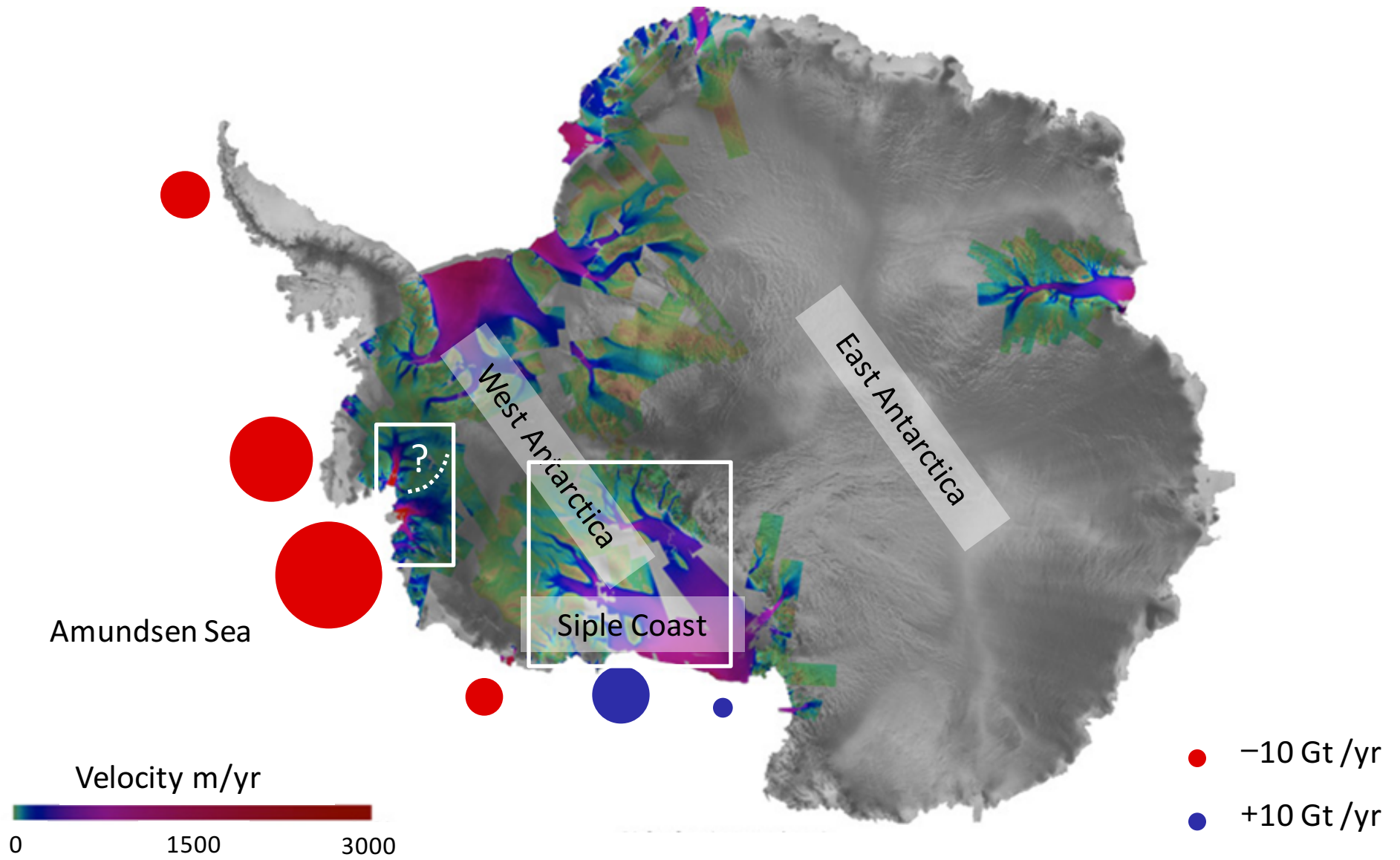
$$F = \int_0^{y_{\max}} \rho u(x = x_{\text{obs}}) \cdot h \, dy$$





$\tau_* = f(\sigma_n - p)$





Fluid solver

$$\rho(\mathbf{x}) \left(\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} \right) = -\nabla p + \nabla \cdot [\mu(\mathbf{x})(\nabla \mathbf{v} + \nabla \mathbf{v}^T)] \\ + \mathbf{g}\rho(\mathbf{x}) - \sigma\kappa(\mathbf{x})\delta(\mathbf{x})\mathbf{n}$$

$$\nabla \cdot \mathbf{v} = 0$$

$$[p] = \sigma\kappa + 2[\mu](\nabla u \cdot \mathbf{n}, \nabla v \cdot \mathbf{n}, \nabla w \cdot \mathbf{n}) \cdot \mathbf{n}$$

Interface solver

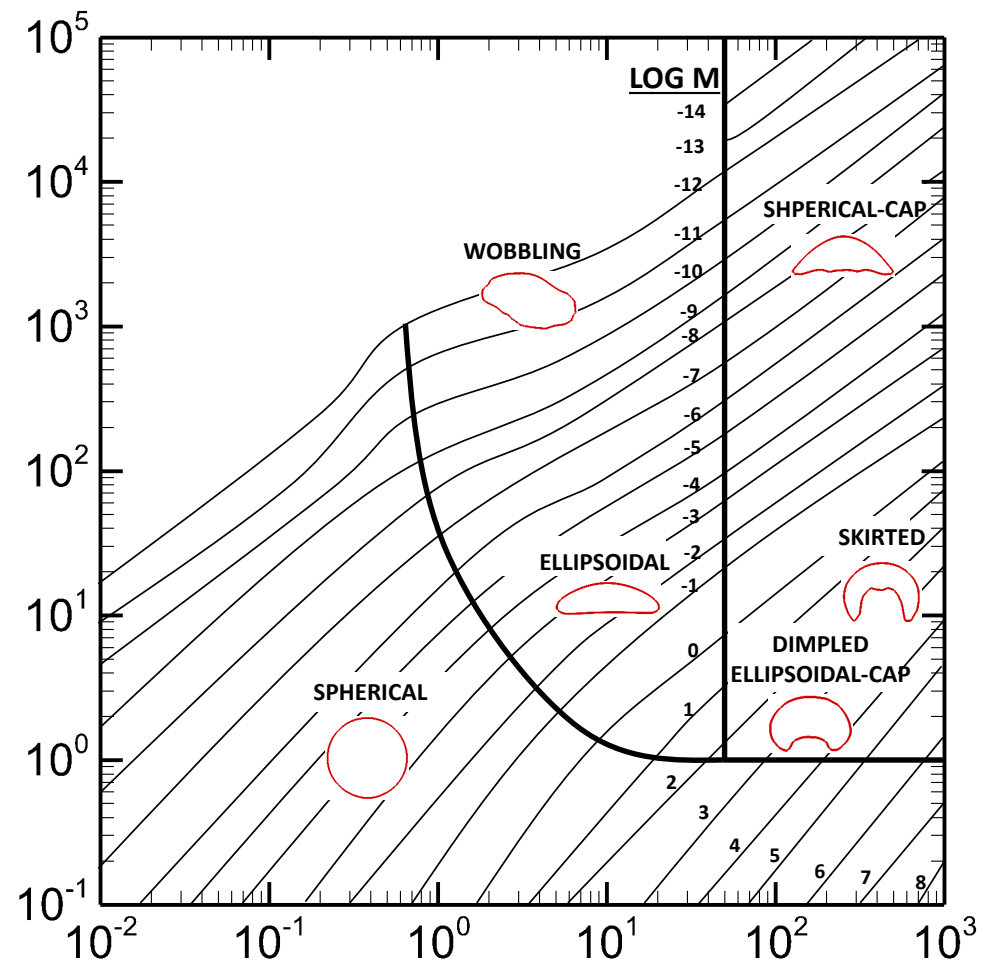
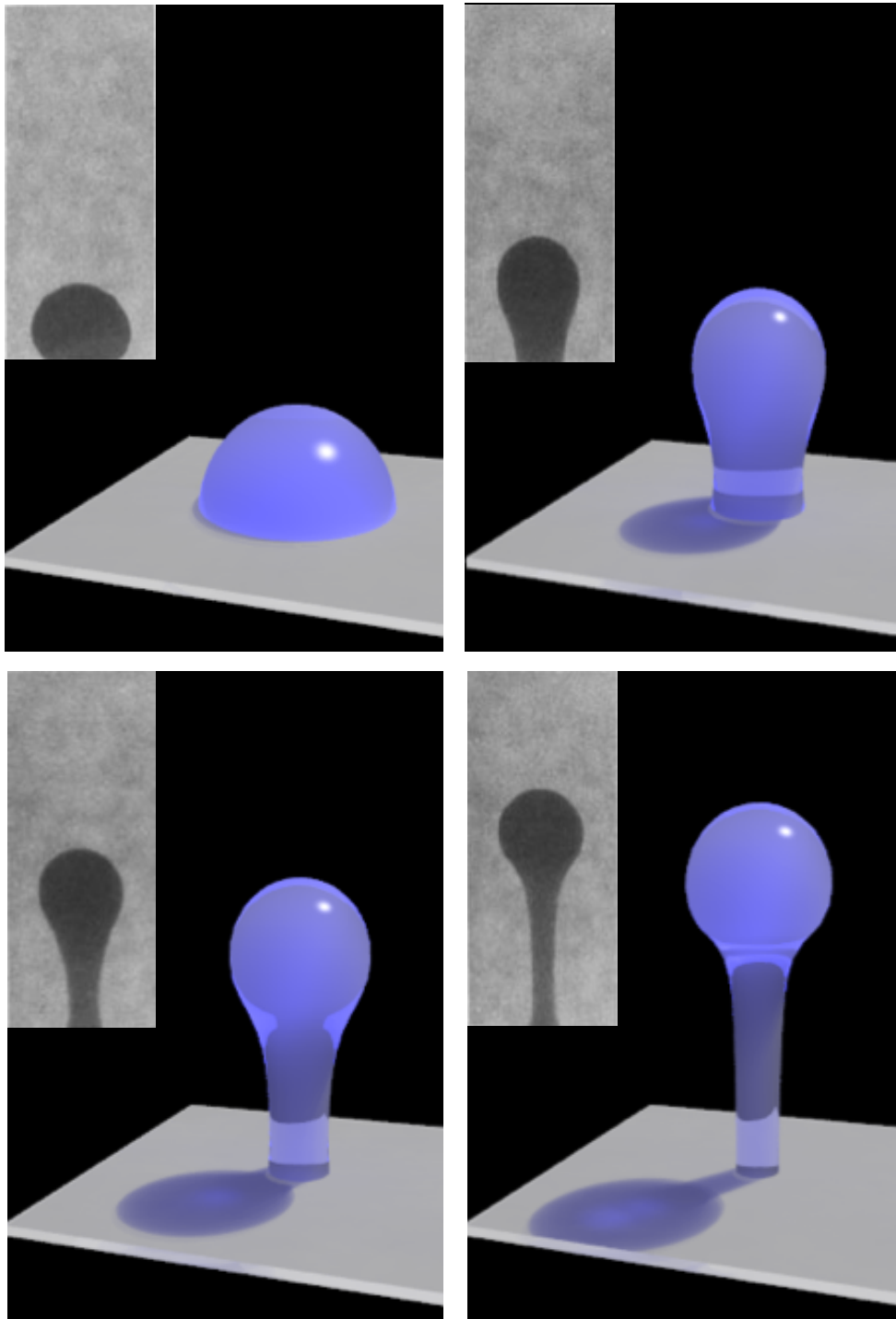
$$\frac{\partial \phi}{\partial t} + \mathbf{v} \cdot \nabla \phi = 0$$

Solid solver

$$\frac{d(m_p \vec{U}_p)}{dt} = \vec{F}_p + \vec{g}$$

$$\frac{d(\hat{I}_p \cdot \vec{\omega}_p)}{dt} = \vec{T}_p,$$

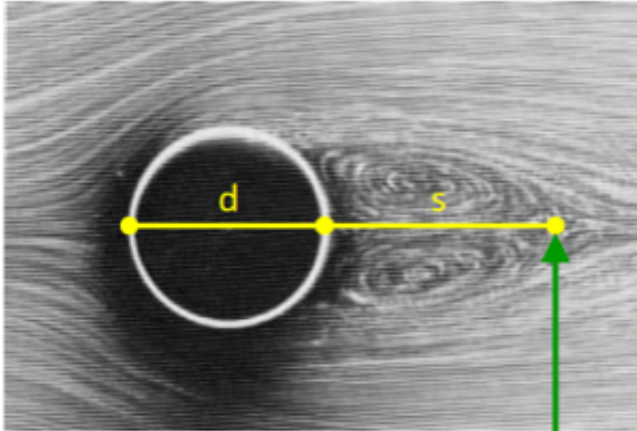
$$\frac{d\vec{X}_p}{dt} = \vec{u}_p$$



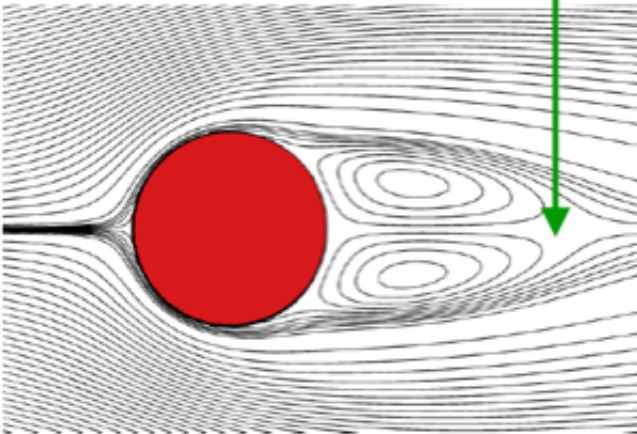
Manga and Stone, 1993; Suckale et al., 2010a; Clift et al., 2005; Qin and Suckale, 2017.

1. Wake formation

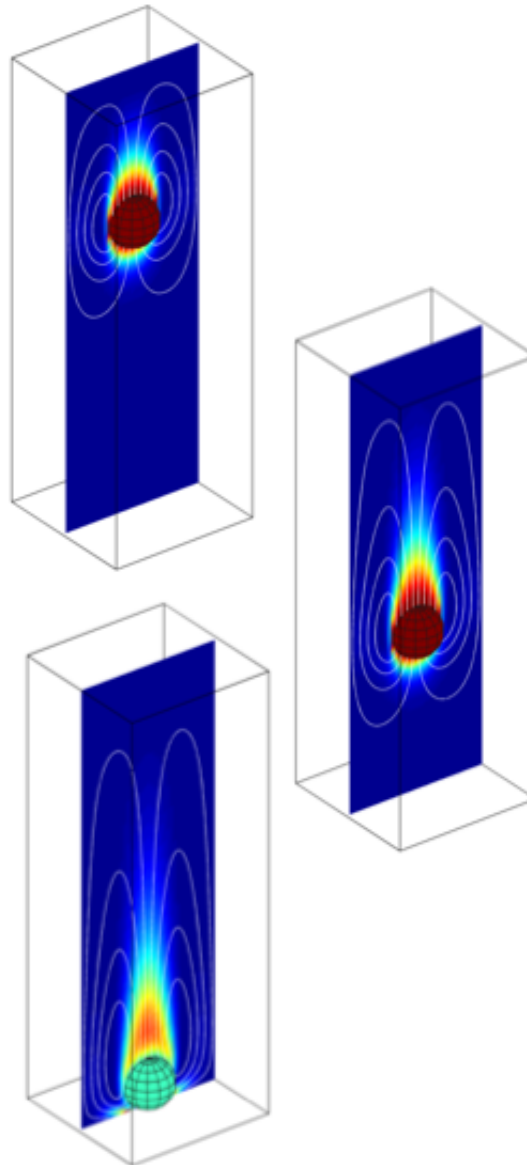
A. Experiment



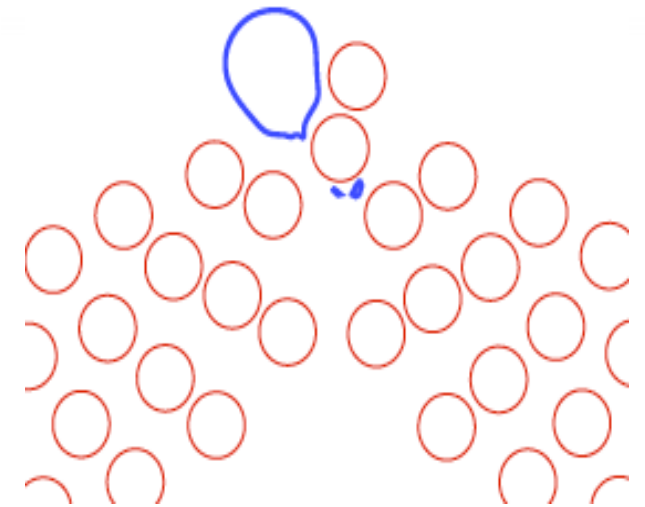
B. Simulation

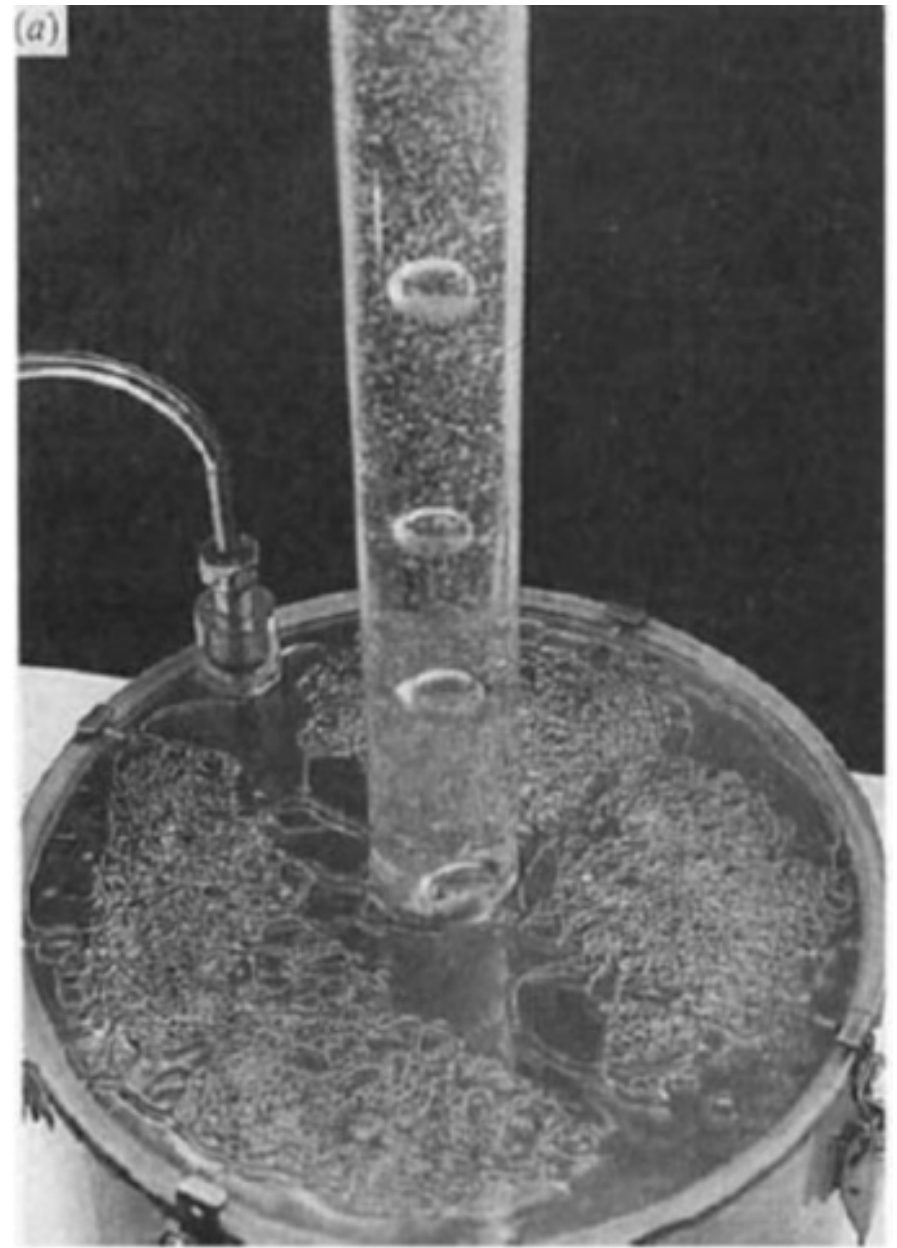
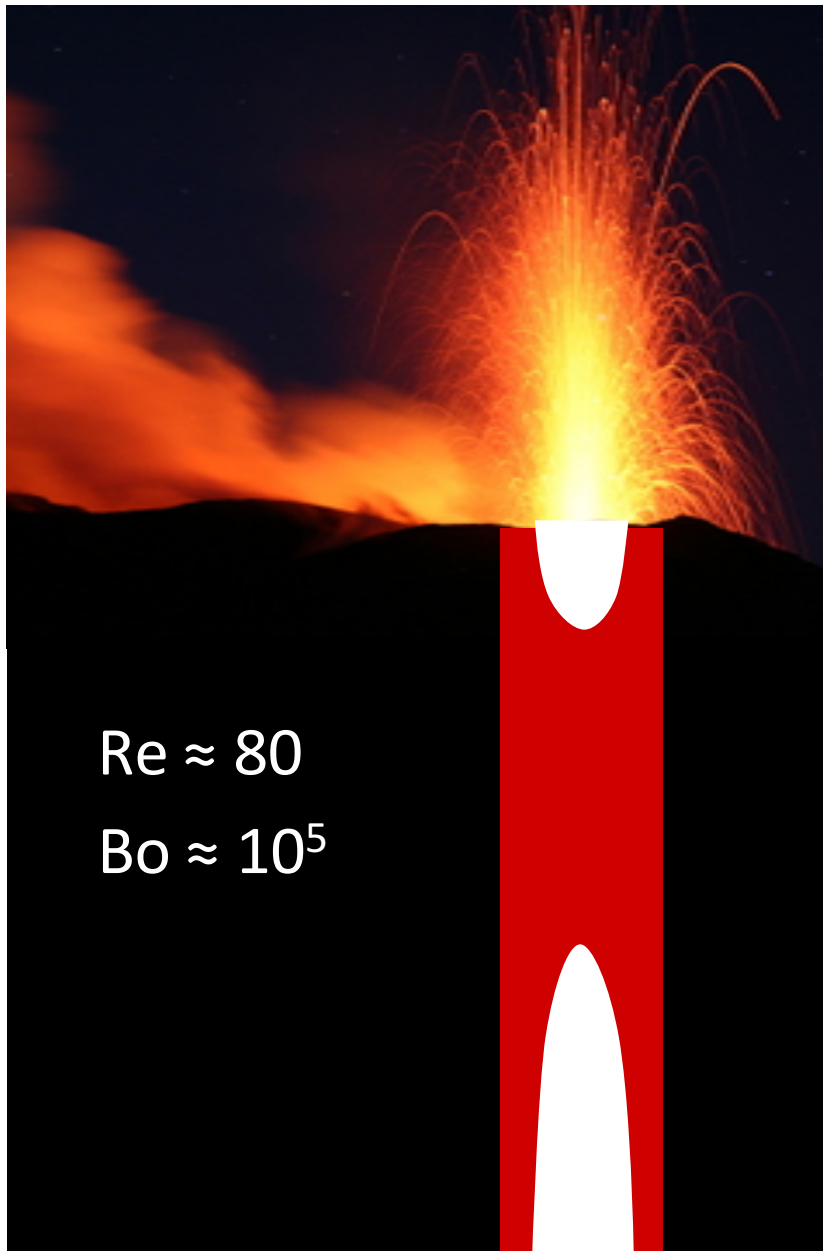


2. Settling speed

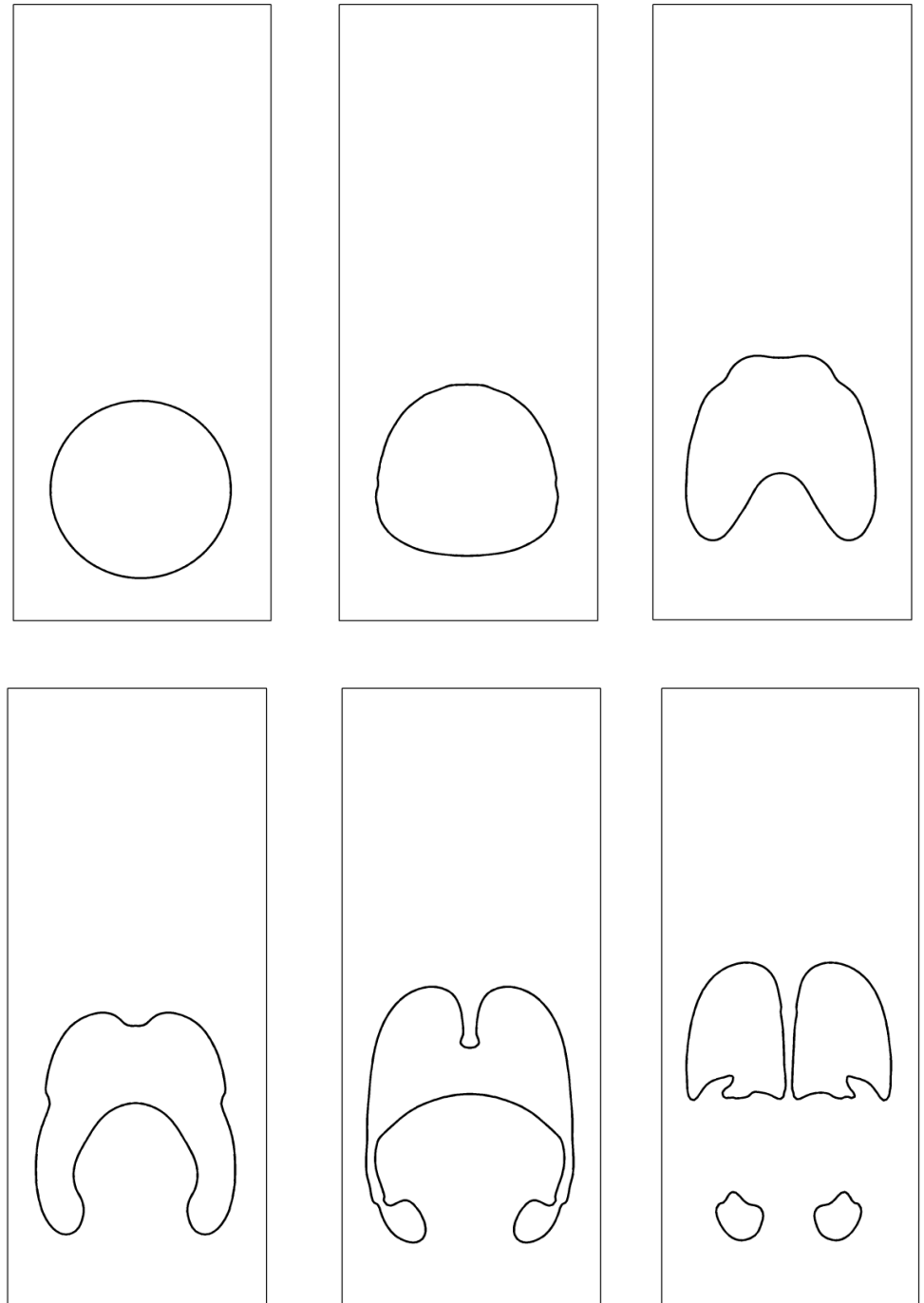
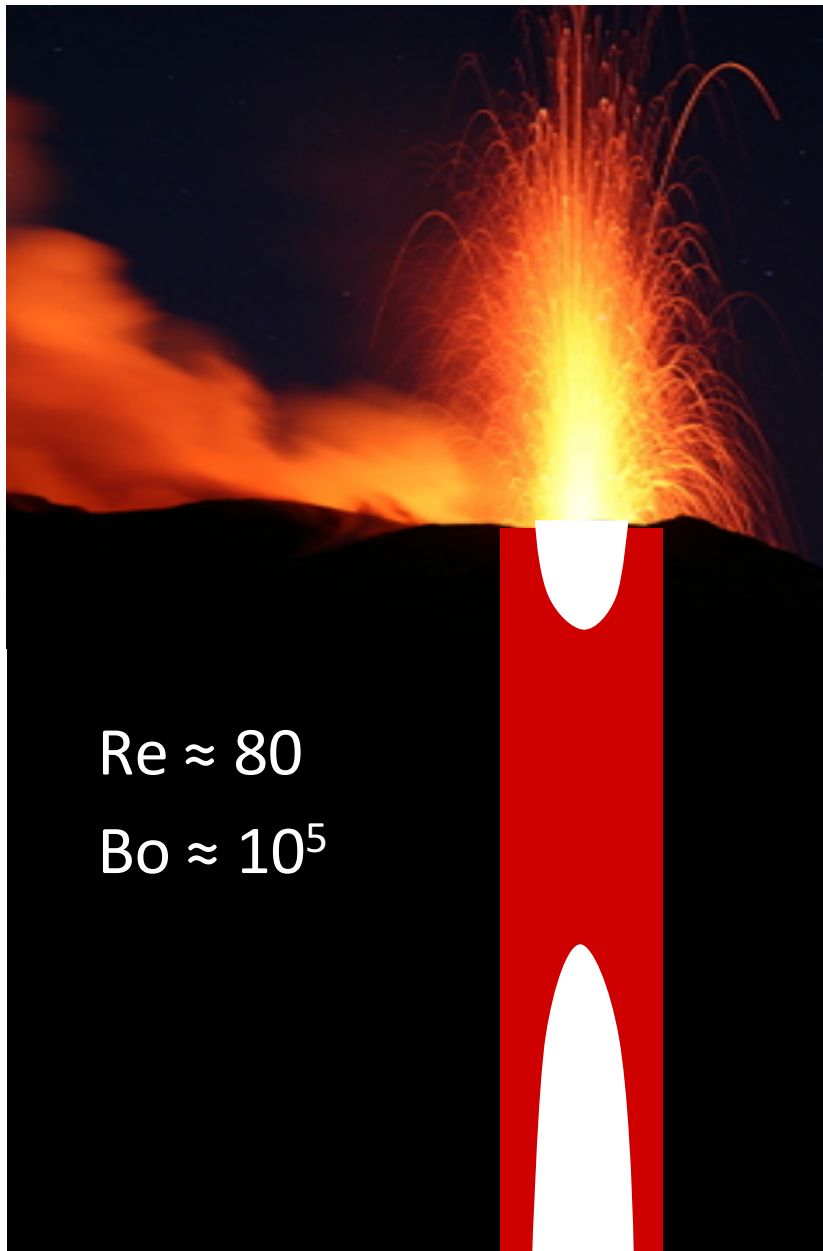


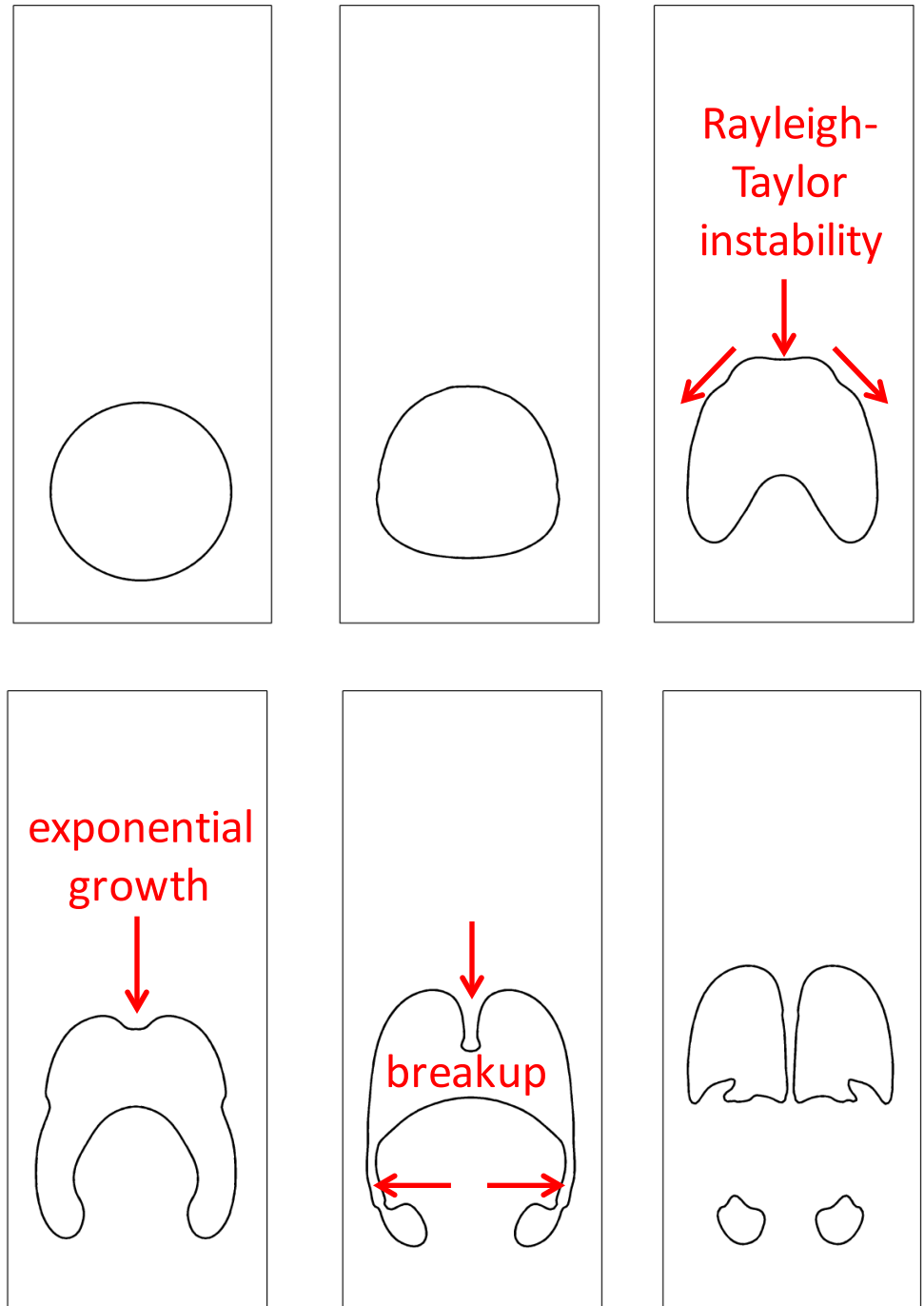
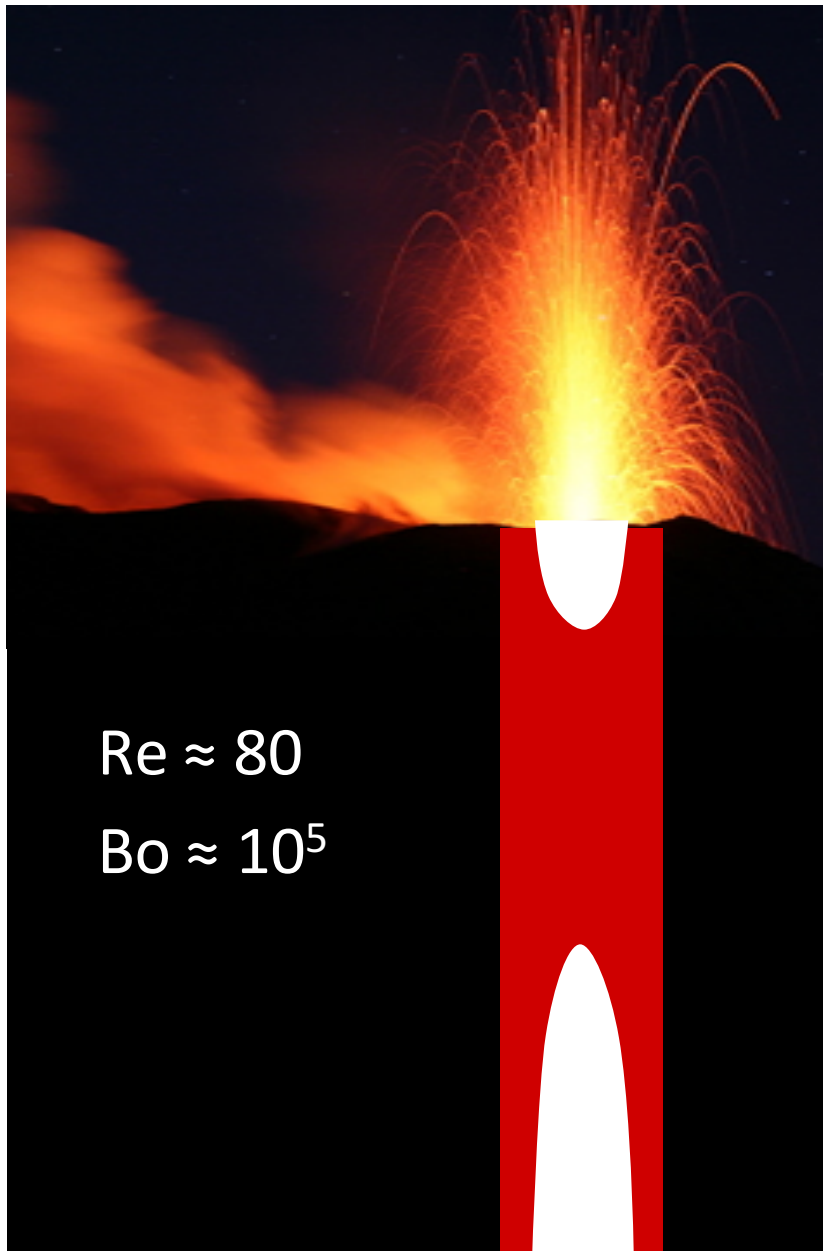
3. Three-phase coupling

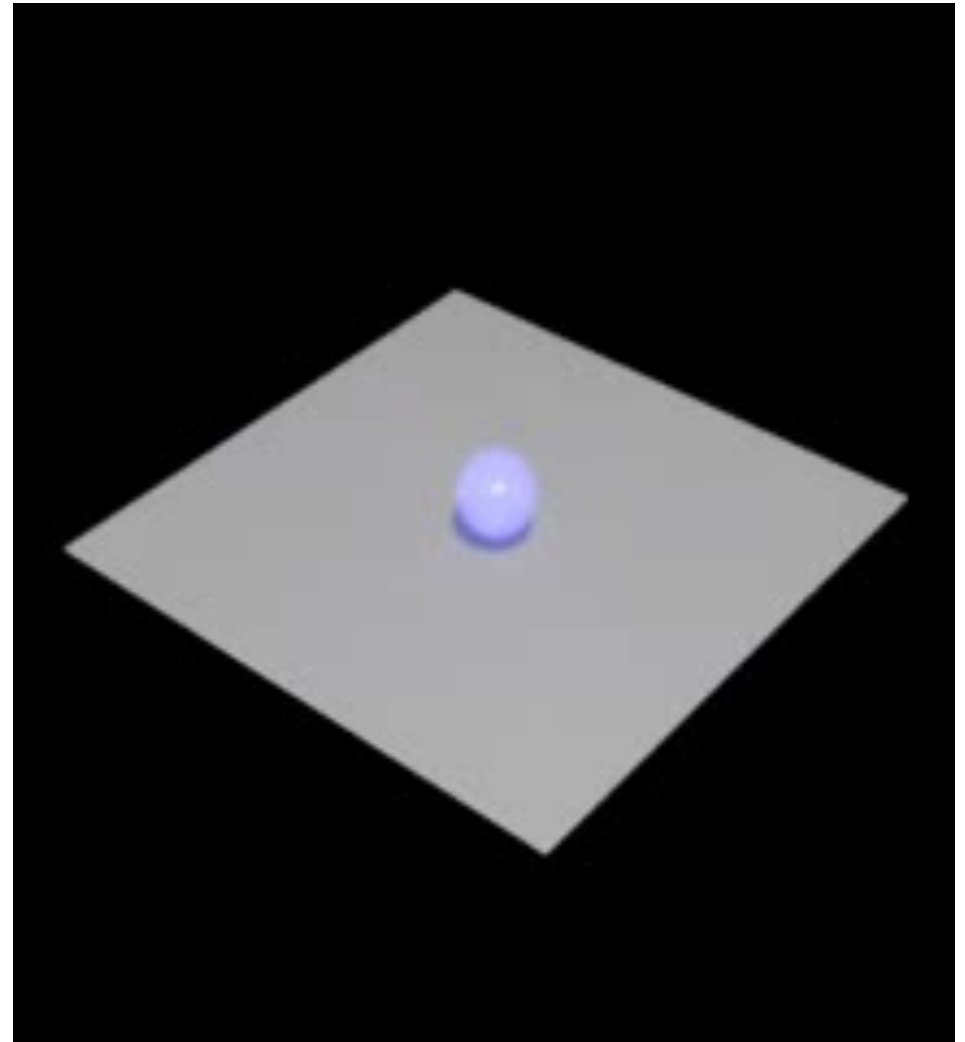
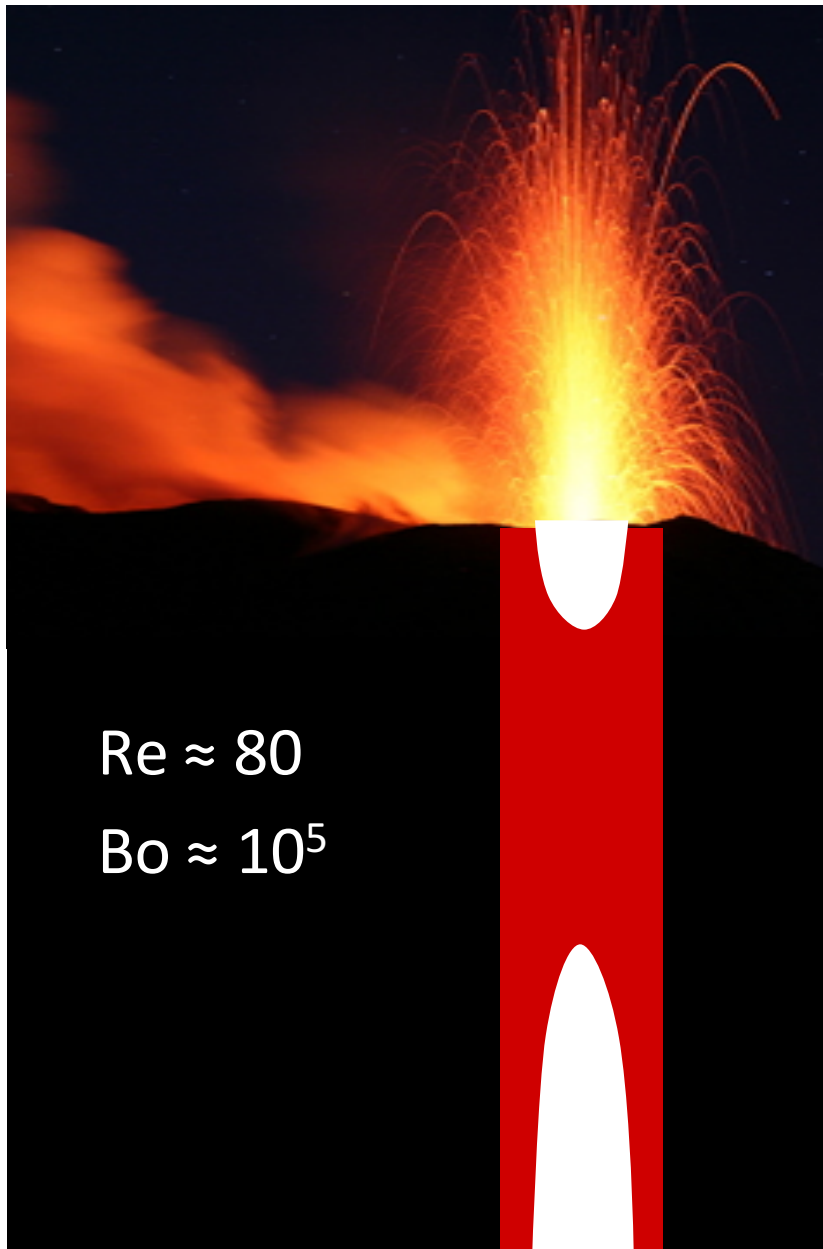




Scaling from Vergniolle et al., 1996; Photo by Jaupart and Vergniolle, 1988;

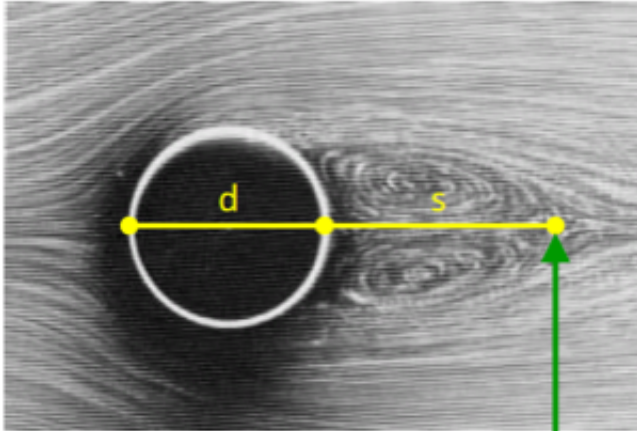




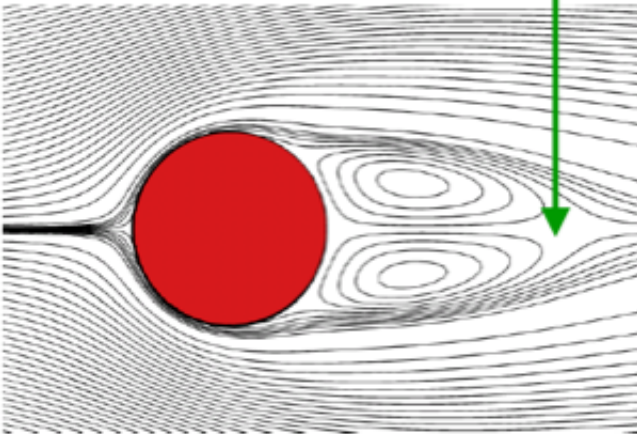


1. Wake formation

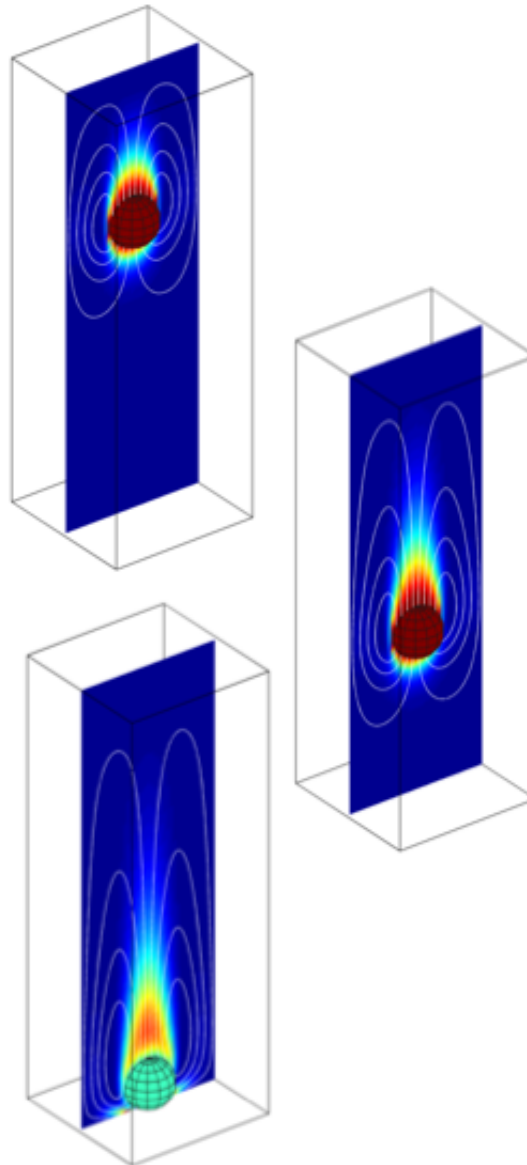
A. Experiment



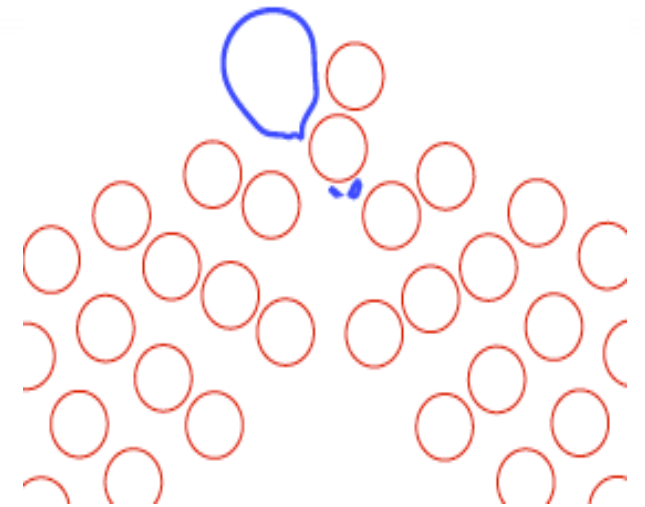
B. Simulation



2. Settling speed



3. Three-phase coupling





Tobias Keller

Governing equations

SEGREGATION

conservation of phase momentum

$$\phi^i \Delta \mathbf{v}^{i*} = -\frac{q_\phi^i}{\eta_\phi^i} \left(\phi^i \nabla P^* + \nabla \phi^i \Delta P^{i*} - \nabla \cdot \phi^i \eta_\phi^i \mathbf{D}(\mathbf{v}^i) - \phi^i \rho^i \mathbf{g} \right)$$

COMPACTION

conservation of phase mass

$$\phi^i \Delta P^{i*} = -\frac{\eta_\phi^i}{r_\phi^i} \left(\phi^i \nabla \cdot \mathbf{v}^* + \nabla \cdot \phi^i \Delta \mathbf{v}^{i*} - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma_\rho^i}{\rho^i} \right)$$

PHASE EVOLUTION

conservation of phase volume

$$\frac{D^i \phi^i}{Dt} = \nabla \cdot \kappa_\phi^i \nabla \Delta \phi^{i*} - \phi^i \nabla \cdot \mathbf{v}^i - \frac{\phi^i}{\rho^i} \frac{D^i \rho^i}{Dt} - \frac{\Gamma_\rho^i}{\rho^i}$$

CHEMICAL EVOLUTION

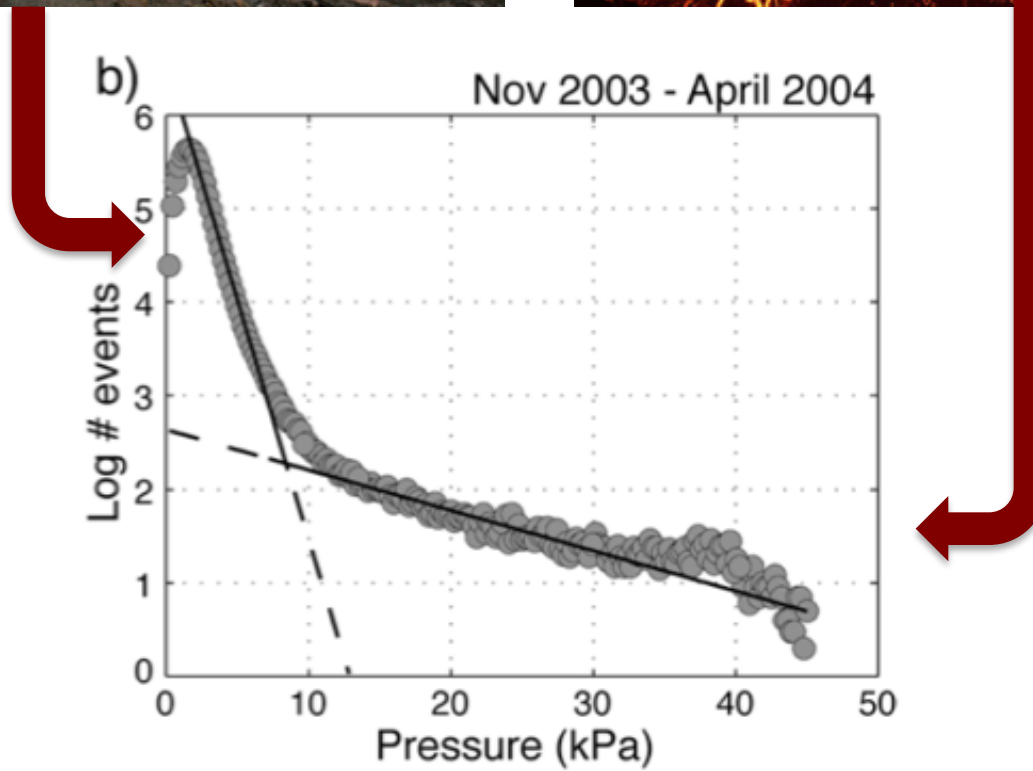
conservation of component mass

$$\frac{D^i c_j^i}{Dt} = \nabla \cdot \kappa_j^i \nabla \Delta c_{j*}^i + \frac{\Delta c_j^{i\Gamma} \Gamma_\rho^i}{\phi^i \rho^i}$$

THERMAL EVOLUTION

conservation of phase energy

$$\frac{D^i T^i}{Dt} = \nabla \cdot \kappa_T^i \nabla T^i - \frac{\kappa_T^i}{d^{i2}} \Delta T^{i*} + \frac{L^{i*} \Gamma_\rho^i}{\phi^i \rho^i c_p^i} + \frac{\Psi^i}{\phi^i \rho^i c_p^i} + \frac{\alpha^i T^i}{\rho^i c_p^i} \frac{D^i P^i}{Dt} + \frac{H^i}{c_p^i}$$



Modified figure 11 from Ripepe et al. 2007